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Ferguson

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(54) **METHOD AND APPARATUS TO CONTROL
DISPLAY BRIGHTNESS WITH AMBIENT
LIGHT CORRECTION**

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This patent is subject to a terminal dis-
claimer.

2,572,258 A	10/1951	Goldfield et al.
2,965,799 A	12/1960	Brooks et al.
2,968,028 A	1/1961	Eilichi et al.
3,141,112 A	7/1964	Eppert
3,449,629 A	6/1969	Wigert et al.
3,565,806 A	2/1971	Ross
3,597,656 A	8/1971	Douglas
3,611,021 A	10/1971	Wallace
3,683,923 A	8/1972	Anderson
3,737,755 A	6/1973	Calkin et al.
3,742,330 A	6/1973	Hodges et al.
3,916,283 A	10/1975	Burrows
3,936,696 A	2/1976	Gray
3,944,888 A	3/1976	Clark
4,053,813 A	10/1977	Komrumpf et al.
4,060,751 A	11/1977	Anderson
4,204,141 A	5/1980	Nuver

(Continued)

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(56) **References Cited**

U.S. PATENT DOCUMENTS

2,429,162 A	10/1947	Russell et al.
2,440,984 A	5/1948	Summers

FOREIGN PATENT DOCUMENTS

EP	0326114	8/1989
----	---------	--------

(Continued)

OTHER PUBLICATIONS

Tannas, Lawrence, "Flat Panel Displays and CRTs". ©1985 Van
Nostrand Reinhold Company Inc., pp. 96-99.

(Continued)

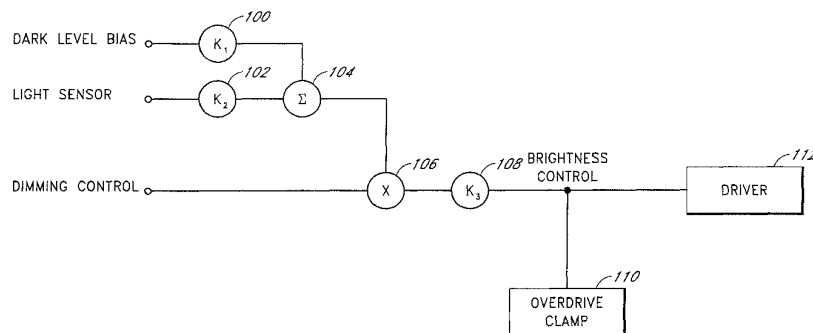
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(57) **ABSTRACT**

An ambient light sensor produces a current signal that varies
linearly with the level of ambient light. The current signal is
multiplied by a user dimming preference to generate a bright-
ness control signal that automatically compensates for ambi-
ent light variations in visual information display systems. The
multiplying function provides noticeable user dimming control
at relatively high ambient light levels.

20 Claims, 10 Drawing Sheets



US 8,223,117 B2

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U.S. PATENT DOCUMENTS

4,277,728 A	7/1981	Stevens	5,485,059 A	1/1996	Yamashita et al.
4,307,441 A	12/1981	Bello	5,485,487 A	1/1996	Orbach et al.
4,353,009 A	10/1982	Knoll	5,493,183 A	2/1996	Kimball
4,386,345 A *	5/1983	Narveson et al. 345/207	5,495,405 A	2/1996	Fujimura et al.
4,388,562 A	6/1983	Josephson	5,510,974 A	4/1996	Gu et al.
4,392,087 A	7/1983	Zansky	5,514,947 A	5/1996	Berg
4,437,042 A	3/1984	Morais et al.	5,519,289 A	5/1996	Katyl et al.
4,441,054 A	4/1984	Bay	5,528,192 A	6/1996	Agiman
4,463,287 A	7/1984	Pitel	5,539,281 A	7/1996	Shackle et al.
4,469,988 A	9/1984	Cronin	5,548,189 A	8/1996	Williams
4,480,201 A	10/1984	Jaeschke	5,552,697 A	9/1996	Chan
4,523,130 A	6/1985	Pitel	5,557,249 A	9/1996	Reynal
4,543,522 A	9/1985	Moreau	5,563,473 A	10/1996	Mattas et al.
4,544,863 A	10/1985	Hashimoto	5,563,501 A	10/1996	Chan
4,555,673 A	11/1985	Huijsing et al.	5,574,335 A	11/1996	Sun
4,562,338 A	12/1985	Okami	5,574,356 A	11/1996	Parker
4,567,379 A	1/1986	Corey et al.	5,608,312 A	3/1997	Wallace
4,572,992 A	2/1986	Masaki	5,612,594 A	3/1997	Maheshwari
4,574,222 A	3/1986	Anderson	5,612,595 A	3/1997	Maheshwari
4,585,974 A	4/1986	Stupp et al.	5,615,093 A	3/1997	Nalbant
4,622,496 A	11/1986	Dattilo et al.	5,619,104 A	4/1997	Eunghwa
4,626,770 A	12/1986	Price, Jr.	5,619,402 A	4/1997	Liu
4,630,005 A	12/1986	Clegg et al.	5,621,281 A	4/1997	Kawabata et al.
4,663,566 A	5/1987	Nagano	5,629,588 A	5/1997	Oda et al.
4,663,570 A	5/1987	Luchaco et al.	5,635,799 A	6/1997	Hesterman
4,672,300 A	6/1987	Harper	5,652,479 A	7/1997	LoCascio et al.
4,675,574 A	6/1987	Delflache	5,663,613 A	9/1997	Yamashita et al.
4,682,080 A	7/1987	Ogawa et al.	5,705,877 A	1/1998	Shimada
4,686,615 A	8/1987	Ferguson	5,710,489 A	1/1998	Nilssen
4,689,802 A	8/1987	McCambridge	5,712,533 A	1/1998	Corti
4,698,554 A	10/1987	Stupp et al.	5,712,776 A	1/1998	Palara et al.
4,700,113 A	10/1987	Stupp et al.	5,719,474 A	2/1998	Vitello
4,713,659 A *	12/1987	Oyagi et al. 345/48	5,744,915 A	4/1998	Nilssen
4,717,863 A	1/1988	Zeiler	5,748,460 A	5/1998	Ishihawa
4,745,339 A	5/1988	Izawa et al.	5,751,115 A	5/1998	Jayaraman et al.
4,761,722 A	8/1988	Pruitt	5,751,120 A	5/1998	Zeitler et al.
4,766,353 A	8/1988	Burgess	5,751,560 A	5/1998	Yokoyama
4,779,037 A	10/1988	LoCascio	5,754,012 A	5/1998	LoCascio
4,780,696 A	10/1988	Jirka	5,754,013 A	5/1998	Praiswater
4,792,747 A	12/1988	Schroeder	5,760,760 A	6/1998	Helms
4,812,781 A	3/1989	Regnier	5,770,925 A	6/1998	Konopka et al.
4,847,745 A	7/1989	Shekhawat	5,777,439 A	7/1998	Hua
4,862,059 A	8/1989	Tominaga et al.	5,786,801 A	7/1998	Ichise
4,885,486 A	12/1989	Shekhawat et al.	5,796,213 A	8/1998	Kawasaki
4,893,069 A	1/1990	Harada et al.	5,808,422 A	9/1998	Venkitasubrahmanian et al.
4,902,942 A	2/1990	El-Hamamsy et al.	5,818,172 A	10/1998	Lee
4,939,381 A	7/1990	Shibata	5,822,201 A	10/1998	Kijima
4,998,046 A	3/1991	Lester	5,825,133 A	10/1998	Conway
5,023,519 A	6/1991	Jensen	5,828,156 A	10/1998	Roberts
5,030,887 A	7/1991	Guisinger	5,844,540 A	12/1998	Terasaki
5,036,255 A	7/1991	McKnight et al.	5,854,617 A	12/1998	Lee et al.
5,049,790 A	9/1991	Herfurth et al.	5,859,489 A	1/1999	Shimada
5,057,808 A	10/1991	Dhyanchand	5,872,429 A	2/1999	Xia et al.
5,083,065 A	1/1992	Sakata et al.	5,880,946 A	3/1999	Biegel
5,089,748 A	2/1992	Ihms	5,883,473 A	3/1999	Li et al.
5,105,127 A	4/1992	Lavaud et al.	5,886,477 A	3/1999	Honbo et al.
5,130,565 A	7/1992	Girmay	5,892,336 A	4/1999	Lin et al.
5,130,635 A	7/1992	Kase	5,901,176 A	5/1999	Lewison
5,173,643 A	12/1992	Sullivan et al.	5,910,709 A	6/1999	Stevanovic et al.
5,220,272 A	6/1993	Nelson	5,910,713 A	6/1999	Nishi et al.
5,235,254 A	8/1993	Ho	5,912,812 A	6/1999	Moriarty, Jr. et al.
5,270,818 A *	12/1993	Ottenstein 348/602	5,914,842 A	6/1999	Sievers
5,289,051 A	2/1994	Zitta	5,923,129 A	7/1999	Henry
5,317,401 A	5/1994	Dupont et al.	5,923,546 A	7/1999	Shimada et al.
5,327,028 A	7/1994	Yum et al.	5,925,988 A	7/1999	Grave et al.
5,349,272 A	9/1994	Rector	5,930,121 A	7/1999	Henry
5,406,305 A	4/1995	Shimomura et al.	5,930,126 A	7/1999	Griffin et al.
5,410,221 A	4/1995	Mattas et al.	5,936,360 A	8/1999	Kaneko
5,420,779 A	5/1995	Payne	5,939,830 A	8/1999	Praiswater
5,430,641 A	7/1995	Kates	6,002,210 A	12/1999	Nilssen
5,434,477 A	7/1995	Crouse et al.	6,011,360 A	1/2000	Gradzki et al.
5,440,208 A	8/1995	Uskaly et al.	6,016,245 A	1/2000	Ross
5,463,287 A	10/1995	Kurihara et al.	6,020,688 A	2/2000	Moisin
5,471,130 A	11/1995	Agiman	6,028,400 A	2/2000	Pol et al.
5,475,284 A	12/1995	Lester et al.	6,037,720 A	3/2000	Wong et al.
5,475,285 A	12/1995	Konopka	6,038,149 A	3/2000	Hiraoka et al.
5,479,337 A	12/1995	Voigt	6,040,661 A	3/2000	Bogdan
5,485,057 A	1/1996	Smallwood et al.	6,040,662 A	3/2000	Asayama
			6,043,609 A	3/2000	George et al.

US 8,223,117 B2

Page 3

6,049,177	A	4/2000	Felper	6,515,881	B2	2/2003	Chou et al.
6,069,448	A	5/2000	Yeh	6,521,879	B1	2/2003	Rand et al.
6,072,282	A	6/2000	Adamson	6,522,558	B2	2/2003	Henry
6,091,209	A	7/2000	Hilgers	6,531,831	B2	3/2003	Chou et al.
6,104,146	A	8/2000	Chou et al.	6,534,934	B1	3/2003	Lin et al.
6,108,215	A	8/2000	Kates et al.	6,559,606	B1	5/2003	Chou et al.
6,111,370	A	8/2000	Parra	6,563,479	B2	5/2003	Weindorf et al.
6,114,814	A	9/2000	Shannon et al.	6,570,344	B2	5/2003	Lin
6,121,733	A	9/2000	Nilssen	6,570,347	B2	5/2003	Kastner
6,127,785	A	10/2000	Williams	6,583,587	B2	6/2003	Ito et al.
6,127,786	A	10/2000	Moisin	6,593,703	B2	7/2003	Sun
6,137,240	A	10/2000	Bogdan	6,628,093	B2	9/2003	Stevens
6,144,359	A *	11/2000	Grave 345/102	6,630,797	B2	10/2003	Qian et al.
6,150,772	A	11/2000	Crane	6,633,138	B2	10/2003	Shannon et al.
6,157,143	A	12/2000	Bigio et al.	6,642,674	B2	11/2003	Liao et al.
6,160,362	A	12/2000	Shone et al.	6,650,514	B2	11/2003	Schmitt
6,169,375	B1	1/2001	Moisin	6,654,268	B2	11/2003	Choi
6,172,468	B1	1/2001	Hollander	6,664,744	B2	12/2003	Dietz
6,181,066	B1	1/2001	Adamson	6,680,834	B2	1/2004	Williams
6,181,083	B1	1/2001	Moisin	6,703,998	B1	3/2004	Kabel et al.
6,181,084	B1	1/2001	Lau	6,707,264	B2	3/2004	Lin et al.
6,188,183	B1	2/2001	Greenwood et al.	6,710,555	B1	3/2004	Terada et al.
6,188,553	B1	2/2001	Moisin	6,717,372	B2	4/2004	Lin et al.
6,194,841	B1	2/2001	Takahashi et al.	6,717,375	B2	4/2004	Noguchi et al.
6,198,234	B1	3/2001	Henry	6,724,602	B2	4/2004	Giannopoulos
6,198,236	B1	3/2001	O'Neill	6,765,354	B2	7/2004	Klien
6,211,625	B1	4/2001	Nilssen	6,781,325	B2	8/2004	Lee
6,215,256	B1	4/2001	Ju	6,784,627	B2	8/2004	Suzuki et al.
6,218,788	B1	4/2001	Chen et al.	6,803,901	B1	10/2004	Numao
6,229,271	B1	5/2001	Liu	6,804,129	B2	10/2004	Lin
6,239,558	B1	5/2001	Fujimura et al.	6,809,718	B2	10/2004	Wei et al.
6,252,355	B1	6/2001	Meldrum et al.	6,809,938	B2	10/2004	Lin et al.
6,255,784	B1	7/2001	Weindorf	6,815,906	B1	11/2004	Aarons et al.
6,259,215	B1	7/2001	Roman	6,816,142	B2	11/2004	Oda et al.
6,259,615	B1	7/2001	Lin	6,856,099	B2	2/2005	Chen et al.
6,281,636	B1	8/2001	Okutsu et al.	6,856,519	B2	2/2005	Lin et al.
6,281,638	B1	8/2001	Moisin	6,864,867	B2	3/2005	Biebl
6,291,946	B1	9/2001	Hinman	6,870,330	B2	3/2005	Choi
6,294,883	B1	9/2001	Weindorf	6,876,157	B2	4/2005	Henry
6,307,765	B1	10/2001	Choi	6,897,698	B1	5/2005	Gheorghiu et al.
6,310,444	B1	10/2001	Chang	6,900,599	B2	5/2005	Ribarich
6,313,586	B1	11/2001	Yamamoto et al.	6,900,600	B2	5/2005	Rust et al.
6,316,881	B1	11/2001	Shannon et al.	6,900,993	B2	5/2005	Lin et al.
6,316,887	B1	11/2001	Ribarich et al.	6,922,023	B2	7/2005	Hsu et al.
6,317,347	B1	11/2001	Weng	6,930,893	B2	8/2005	Vinciarelli
6,320,329	B1	11/2001	Wacyk	6,936,975	B2	8/2005	Lin et al.
6,323,602	B1	11/2001	De Groot et al.	6,947,024	B2	9/2005	Lee et al.
6,331,755	B1	12/2001	Ribarich et al.	6,967,449	B2	11/2005	Ishihara
6,340,870	B1	1/2002	Yamashita et al.	6,967,657	B2	11/2005	Lowles et al.
6,344,699	B1	2/2002	Rimmer	6,969,958	B2	11/2005	Henry
6,351,080	B1	2/2002	Birk et al.	6,979,959	B2	12/2005	Henry
6,356,035	B1	3/2002	Weng	7,026,860	B1	4/2006	Gheorghiu et al.
6,359,393	B1	3/2002	Brown	7,057,611	B2	6/2006	Lin et al.
6,362,577	B1	3/2002	Ito et al.	7,075,245	B2	7/2006	Liu
6,388,388	B1	5/2002	Weindorf et al.	7,095,392	B2	8/2006	Lin
6,396,217	B1	5/2002	Weindorf	7,120,035	B2	10/2006	Lin et al.
6,396,722	B2	5/2002	Lin	7,151,394	B2	12/2006	Gheorghiu et al.
6,417,631	B1	7/2002	Chen et al.	7,183,724	B2	2/2007	Ball
6,420,839	B1	7/2002	Chiang et al.	7,187,140	B2	3/2007	Ball
6,424,100	B1	7/2002	Kominami et al.	7,190,123	B2	3/2007	Lee
6,429,839	B1	8/2002	Sakamoto	7,202,458	B2	4/2007	Park
6,433,492	B1	8/2002	Buonavita	7,233,117	B2	6/2007	Wang et al.
6,441,943	B1	8/2002	Roberts et al.	7,236,020	B1	6/2007	Virgil
6,445,141	B1	9/2002	Kastner et al.	7,468,722	B2	12/2008	Ferguson
6,452,344	B1	9/2002	MacAdam et al.	7,755,595	B2	7/2010	Ferguson
6,459,215	B1	10/2002	Nerone et al.	2001/0036096	A1	11/2001	Lin
6,459,216	B1	10/2002	Tsai	2002/0030451	A1	3/2002	Moisin
6,469,922	B2	10/2002	Choi	2002/0097004	A1	7/2002	Chiang et al.
6,472,827	B1	10/2002	Nilssen	2002/0114114	A1	8/2002	Schmitt
6,472,876	B1	10/2002	Notohamiprodjo et al.	2002/0118182	A1	8/2002	Weindorf
6,479,810	B1	11/2002	Weindorf	2002/0130786	A1	9/2002	Weindorf
6,483,245	B1	11/2002	Weindorf	2002/0135319	A1	9/2002	Bruning et al.
6,486,618	B1	11/2002	Li	2002/0140538	A1	10/2002	Yer
6,494,587	B1	12/2002	Shaw et al.	2002/0145886	A1	10/2002	Stevens
6,495,972	B1	12/2002	Okamoto et al.	2002/0153852	A1	10/2002	Liao et al.
6,501,234	B2	12/2002	Lin et al.	2002/0171376	A1	11/2002	Rust et al.
6,507,286	B2	1/2003	Weindorf et al.	2002/0180380	A1	12/2002	Lin
6,509,696	B2	1/2003	Bruning et al.	2002/0180572	A1	12/2002	Kakehashi et al.
6,515,427	B2	2/2003	Oura et al.	2002/0181260	A1	12/2002	Chou et al.

2002/0195971	A1	12/2002	Qian et al.
2003/0001524	A1	1/2003	Lin et al.
2003/0020677	A1	1/2003	Nakano
2003/0025462	A1	2/2003	Weindorf
2003/0080695	A1	5/2003	Ohsawa
2003/0090913	A1	5/2003	Che-Chen et al.
2003/0117084	A1	6/2003	Stack
2003/0141829	A1	7/2003	Yu
2003/0161164	A1	8/2003	Shannon et al.
2003/0227435	A1	12/2003	Hsieh
2004/0000879	A1	1/2004	Lee
2004/0012556	A1	1/2004	Yong et al.
2004/0017348	A1	1/2004	Numao
2004/0032223	A1	2/2004	Henry
2004/0051473	A1	3/2004	Jales et al.
2004/0095402	A1*	5/2004	Nakano 346/102
2004/0145558	A1	7/2004	Cheng
2004/0155596	A1	8/2004	Ushijima
2004/0155853	A1	8/2004	Lin
2004/0189217	A1	9/2004	Ishihara et al.
2004/0227719	A1	11/2004	Chang et al.
2004/0257003	A1	12/2004	Hsieh et al.
2004/0263092	A1	12/2004	Liu
2005/0057484	A1	3/2005	Diefenbaugh et al.
2005/0062436	A1	3/2005	Jin
2005/0093471	A1	5/2005	Jin
2005/0093472	A1	5/2005	Jin
2005/0093482	A1	5/2005	Ball
2005/0093483	A1	5/2005	Ball
2005/0093484	A1	5/2005	Ball
2005/0099143	A1	5/2005	Kohn
2005/0156536	A1	7/2005	Ball
2005/0156539	A1	7/2005	Ball
2005/0156540	A1	7/2005	Ball
2005/0162098	A1	7/2005	Ball
2005/0218825	A1	10/2005	Chiou
2005/0225261	A1	10/2005	Jin
2006/0022612	A1	2/2006	Henry
2006/0049959	A1	3/2006	Sanchez
2006/0158136	A1	7/2006	Chen
2009/0091560	A1	4/2009	Ferguson

FOREIGN PATENT DOCUMENTS

EP	0587923	3/1994
EP	0597661	5/1994
EP	0647021	9/1994
JP	06168791	6/1994
JP	8-204488	8/1996
KR	10-2003-0075461	10/2003
TW	554643	9/2003
TW	8-204488	12/2003
TW	200501829	1/2005
WO	WO 94/15444	7/1994
WO	WO 98/09369	3/1998
WO	WO 9941953	8/1999
WO	WO 0237904	5/2002

OTHER PUBLICATIONS

Jordan et al., Resonant Fluorescent Lamp Converter Provides Efficient and Compact Solution, Mar. 1993, pp. 424-431.

UNITRODE Datasheet, Resonant Fluorescent Lamp Driver, UC 1871/2871/3871, May 1993, pp. 1-6.

UNITRODE Product & Applications Handbook 1993-94, U-141, Jun. 1993, pp. i-ii; 9-471-9-478.

Williams, Jim, Techniques for 92% Efficient LCD Illumination, Linear Technology Application Note 55, Aug. 1993.

UNITRODE Datasheet, Resonant Fluorescent Lamp Driver, UC 1871/2871/3871, Oct. 1994, pp. 1-6.

O'Connor, J., Dimmable Cold-Cathode Fluorescent Lamp Ballast Design Using the UC3871, Application Note U-148, pp. 1-15, 1995.

Goodenough, Frank, DC-to-AC Inverter Ups CCFL Lumens Per Watt, Electronic Design, Jul. 10, 1995, pp. 143-148.

Coles, Single Stage CCFL Backlight Resonant Inverter using PWM Dimming Methods, 1998, pp. 35-38.

Micro Linear, ML4878 Single-Stage CCFL Backlight Resonant Inverter, Application Note 68, May 1998, pp. 1-12.

Williams, B.W.; "Power Electronics Devices, Drivers, Applications and Passive Components"; Second Edition, McGraw-Hill, 1992; Chapter 10, pp. 218-249.

Bradley, D.A., "Power Electronics" 2nd Edition; Chapman & Hall, 1995; Chapter 1, pp. 1-38.

Dubey, G. K., "Thyristorised Power Controllers"; Halsted Press, 1986; pp. 74-77.

IEEE Publication, "Dual Switched Mode Power Converter": Pallab Midya & Fred H. Schlereth; p. 155 1989.

IEEE Publication, "High Frequency Resonant Inverter for Group Dimming Control of Fluorescent Lamp Lighting Systems", K.H. Jee, et al., 1989 149-154.

Int. J. Electronics, "New soft-switching inverter for high efficiency electronic ballast with simple structure" E.C. Nho, et al., 1991, vol. 71, No. 3, 529-541.

Nguyen, Don J., "Optimizing Mobile Power Delivery". Presented at Intel Developers Forum, Fall 2001, p. 4.

Plaintiff O2 Micro International Limited's Preliminary Invalidity Contentions re Third-Party Defendant Microsemi Corporation Patents, dated Sep. 14, 2007.

Third-Party Defendant Microsemi Corporation's Brief in Support of its Claim Construction for U.S. Patent Nos. 5,930,121 and 6,198,234, dated Oct. 19, 2007.

Declaration of Irfan A. Lateef in Support of Third-Party Defendant Microsemi Corporation's Brief in Support of its Claim Construction for U.S. Patent Nos. 5,930,121 and 6,198,234, dated Oct. 19, 2007.

Plaintiff O2 Micro International Limited's Brief in Response to Third-Party Defendant Microsemi Corporation's Brief Re Claim Construction for U.S. Patent Nos. 5,930,121 and 6,198,234, dated Oct. 26, 2007.

Declaration of Henry C. Su in Support of Plaintiff O2 Micro International Limited's Brief in Response to Third-Party Defendant Microsemi Corporation's Brief Re Claim Construction for U.S. Patent Nos. 5,930,121 and 6,198,234, dated Oct. 26, 2007.

Defendant/Counterclaimant Monolithic Power Systems, Inc.'s Notice of Motion and Motion for Summary Judgment of Invalidity of Asserted Claims of U. S. Patent No. 6,198,234, dated Nov. 14, 2005.

Defendant/Counterclaimant Monolithic Power Systems, Inc.'s Memorandum of Points and Authorities in Support of Motion for Summary Judgment of Invalidity of Asserted Claims of U. S. Patent No. 6,198,234, dated Nov. 14, 2005.

Declaration of Robert Mammanno filed by Defendant/Counterclaimant Monolithic Power Systems, Inc.'s in Support of Its Motion for Summary Judgment of Invalidity of Asserted Claims of U. S. Patent No. 6,198,234, dated Nov. 14, 2005.

Declaration of John A. O'Connor filed by Defendant/Counterclaimant Monolithic Power Systems, Inc.'s in Support of Its Motion for Summary Judgment of Invalidity of Asserted Claims of U. S. Patent No. 6,198,234, dated Nov. 14, 2005.

Declaration of Defendant/Counterclaimant Monolithic Power Systems, Inc.'s Expert Witness, Dr. Douglas C. Hopkins, In Support of Its Motion for Summary Judgment of Invalidity of Asserted Claims of U. S. Patent No. 6,198,234, dated Nov. 14, 2005.

Declaration of Doyle Slack filed by Defendant/Counterclaimant Monolithic Power Systems, Inc.'s in Support of Its Motion for Summary Judgment of Invalidity of Asserted Claims of U. S. Patent No. 6,198,234, dated Nov. 14, 2005.

Declaration of Dean G. Dunlavey filed by Defendant/Counterclaimant Monolithic Power Systems, Inc.'s in Support of Its Motion for Summary Judgment of Invalidity of Asserted Claims of U. S. Patent No. 6,198,234, dated Nov. 14, 2005.

Declaration of Charles Coles filed by Defendant/Counterclaimant Monolithic Power Systems, Inc.'s in Support of Its Motion for Summary Judgment of Invalidity of Asserted Claims of U. S. Patent No. 6,198,234, dated Nov. 14, 2005.

Plaintiff Microsemi Corporation's Opposition to Defendant/Counterclaimant Monolithic Power Systems, Inc.'s Motion for Summary Judgment of Invalidity of Asserted Claims of U. S. Patent No. 6,198,234, dated Feb. 13, 2006.

Plaintiff Microsemi Corporation's Statement of Genuine Issues in Opposition to Defendant/Counterclaimant Monolithic Power Systems, Inc.'s Motion for Summary Judgment of Invalidity of Asserted Claims of U.S. Patent No. 6,198,234, dated Feb. 13, 2006.

Defendant/Counterclaimant Monolithic Power Systems, Inc.'s Reply Brief in Support of Motion for Summary Judgment of Invalidity of Asserted Claims of U. S. Patent No. 6,198,234, dated Mar. 13, 2006.

Supplemental Declaration of Dean G. Dunlavey filed by Defendant/Counterclaimant Monolithic Power Systems, Inc.'s in Support of Its Motion for Summary Judgment of Invalidity of Asserted Claims of U. S. Patent No. 6,198,234, dated Mar. 13, 2006.

Defendant/Counterclaimant Monolithic Power Systems, Inc.'s Notice of Motion and Motion for Summary Judgment of Invalidity of Asserted Claims of U. S. Patent No. 5,615,093, dated Nov. 14, 2005.

Defendant/Counterclaimant Monolithic Power Systems, Inc.'s Memorandum of Points and Authorities in Support of Motion for Summary Judgment of Invalidity of Asserted Claims of U. S. Patent No. 5,615,093, dated Nov. 14, 2005.

Plaintiff Microsemi Corporation's Opposition to Defendant/Counterclaimant Monolithic Power Systems, Inc.'s Motion for Summary Judgment of Invalidity of Asserted Claims of U.S. Patent No. 5,615,093, dated Feb. 13, 2006.

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Defendant/Counterclaimant Monolithic Power Systems, Inc.'s Reply Brief in Support of Motion for Summary Judgment of Invalidity of Asserted Claims of U. S. Patent No. 5,615,093, dated Mar. 13, 2006.

PCT International Search Report and Written Opinion mailed Apr. 8, 2008, Appl. No. PCT/US2007/072862 in 12 pages.

* cited by examiner

FIG. 1

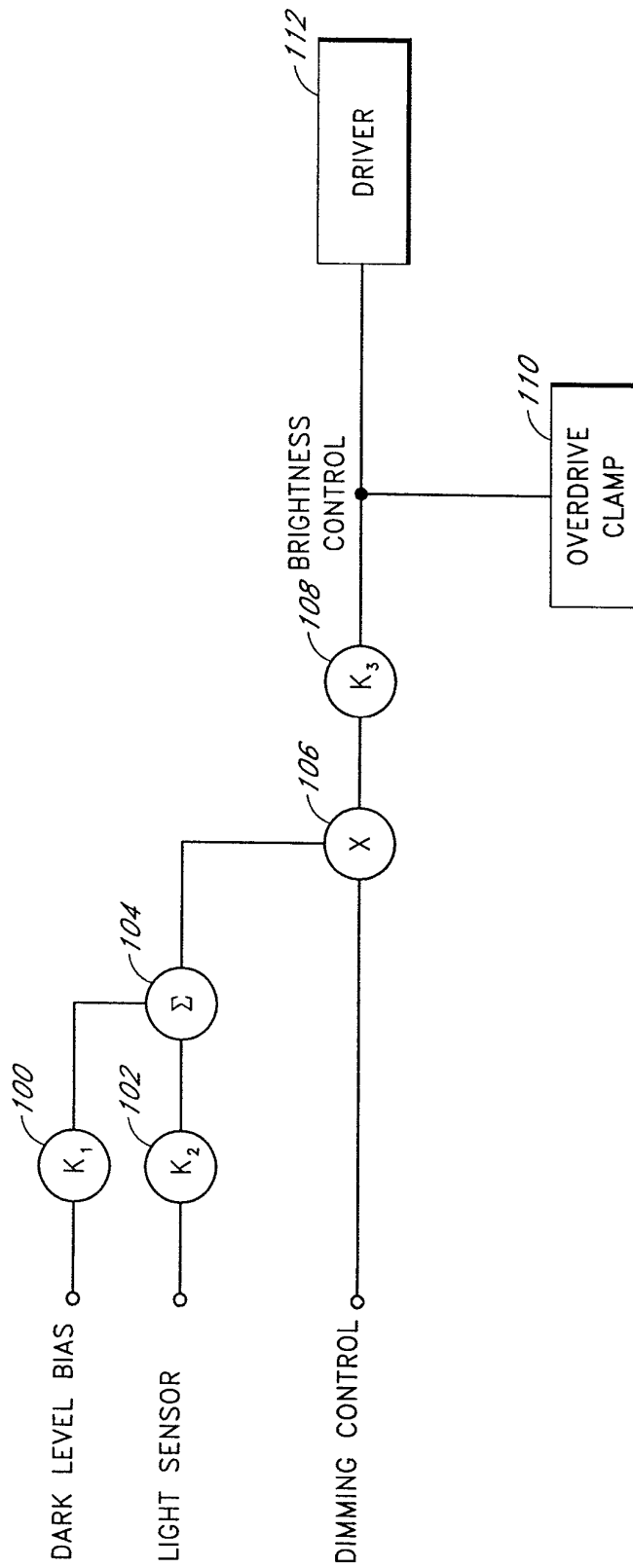


FIG. 2

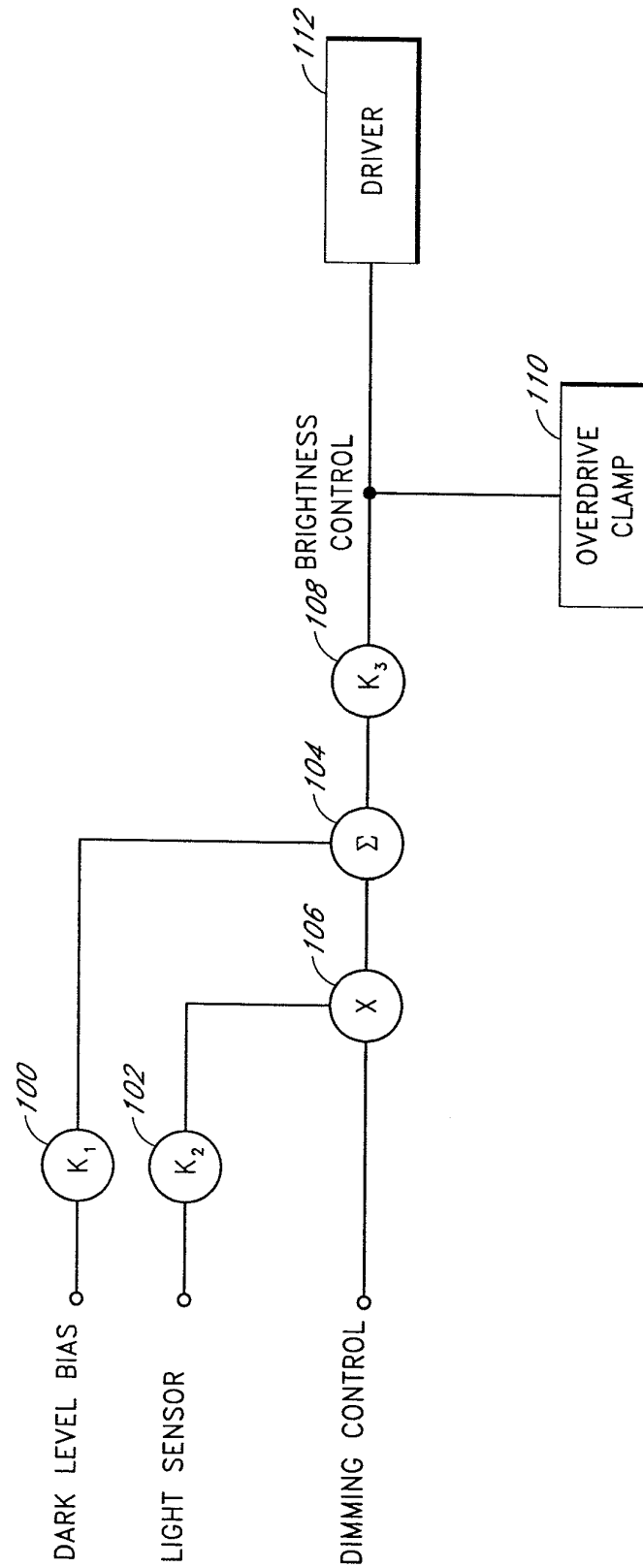


FIG. 3

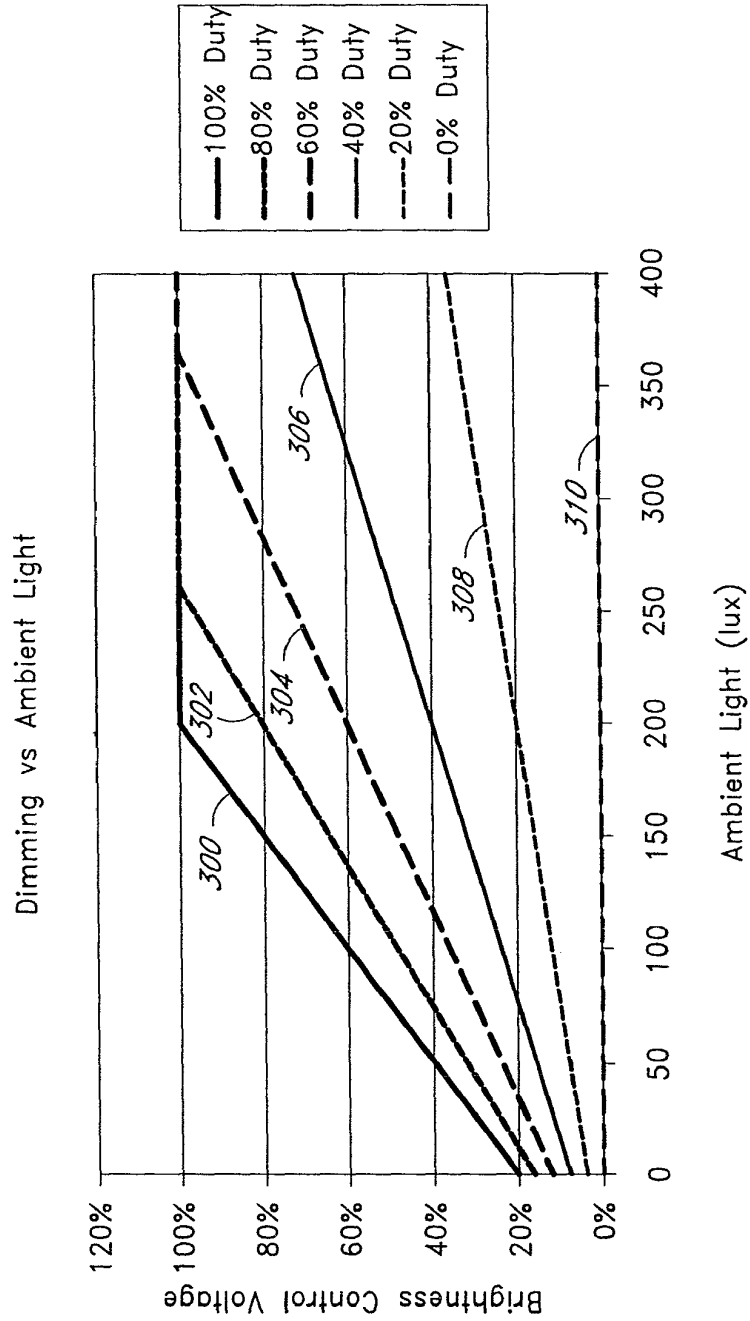


FIG. 4

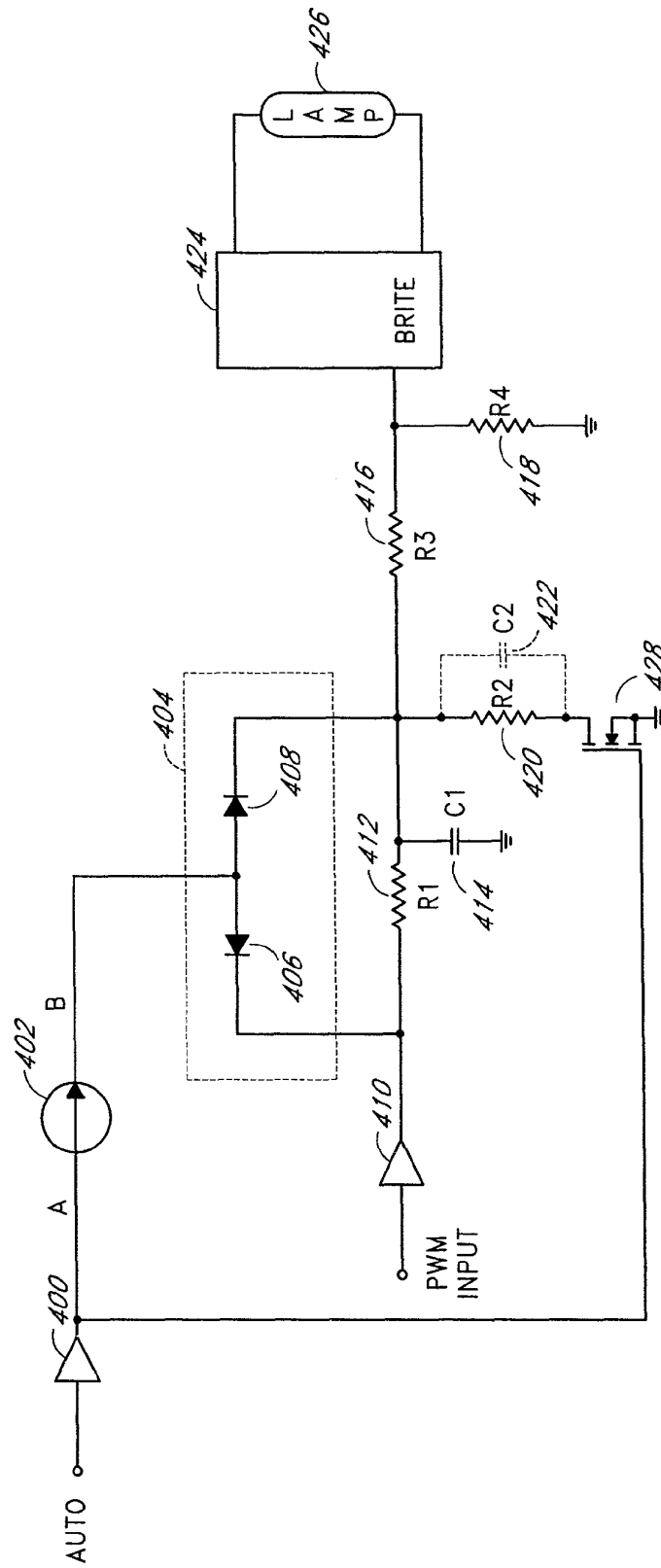


FIG. 5

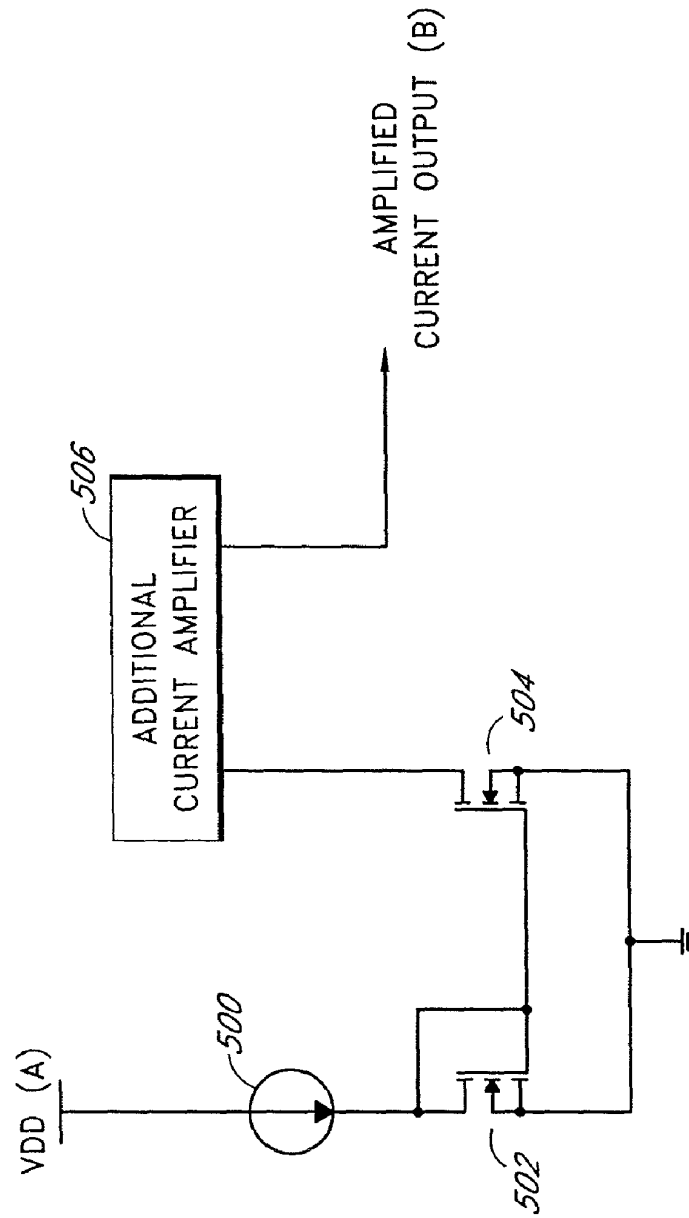


FIG. 6

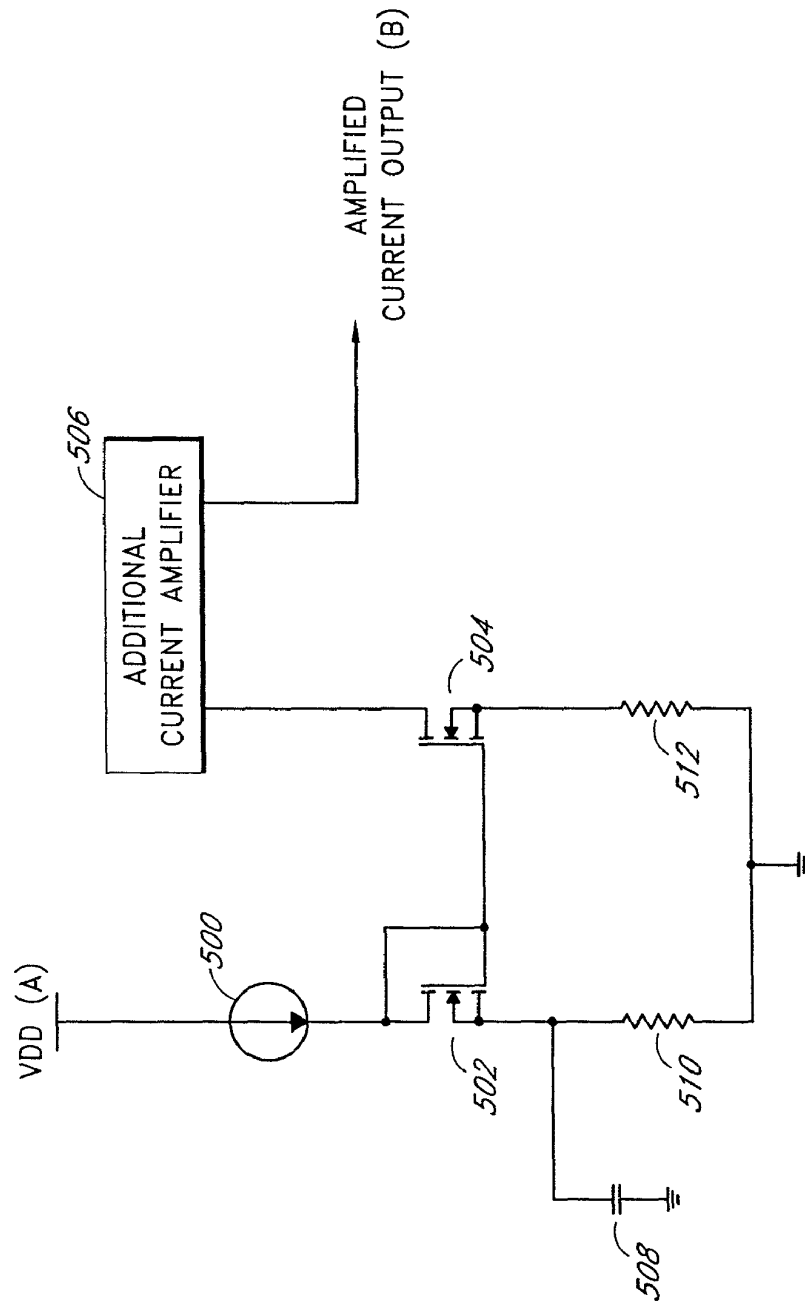


FIG. 7

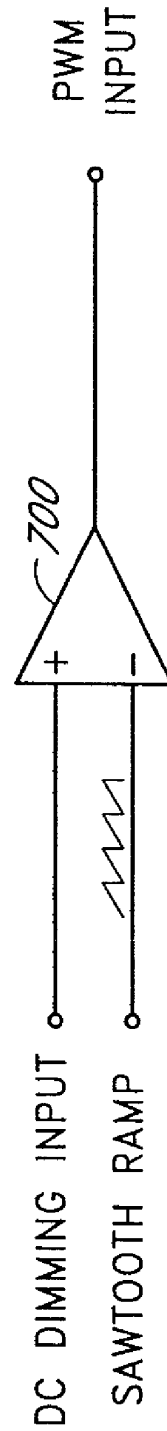


FIG. 8

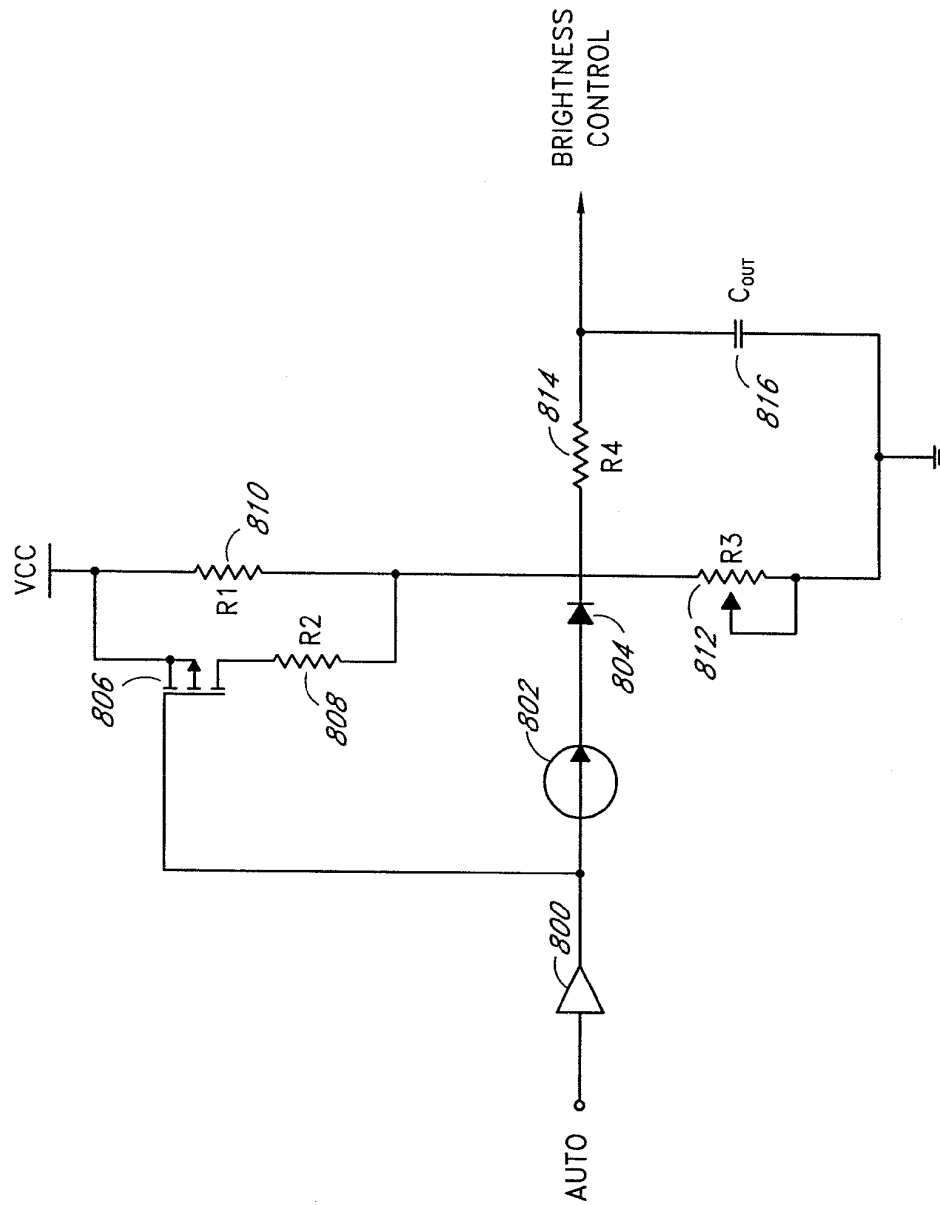


FIG. 9

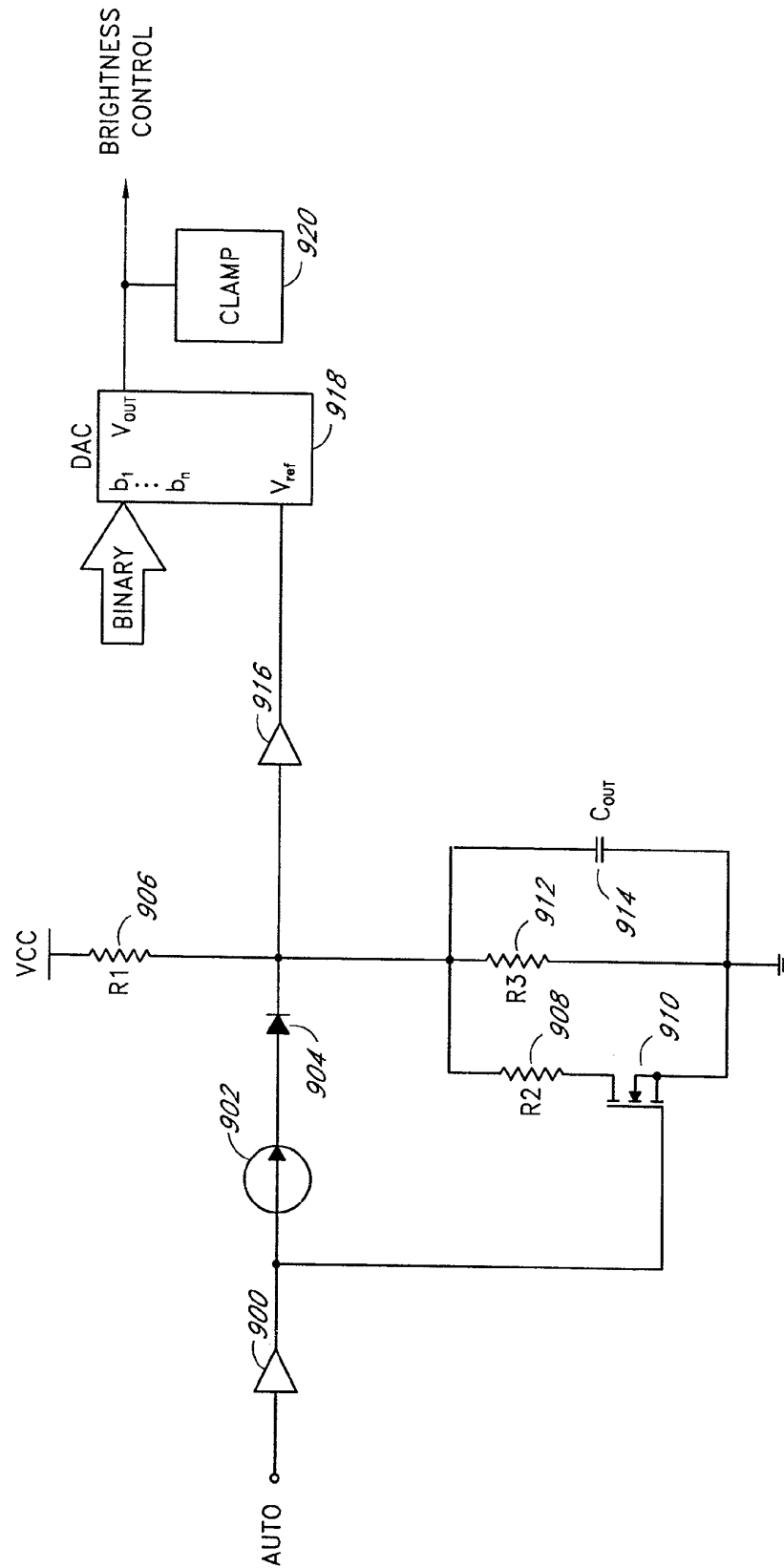
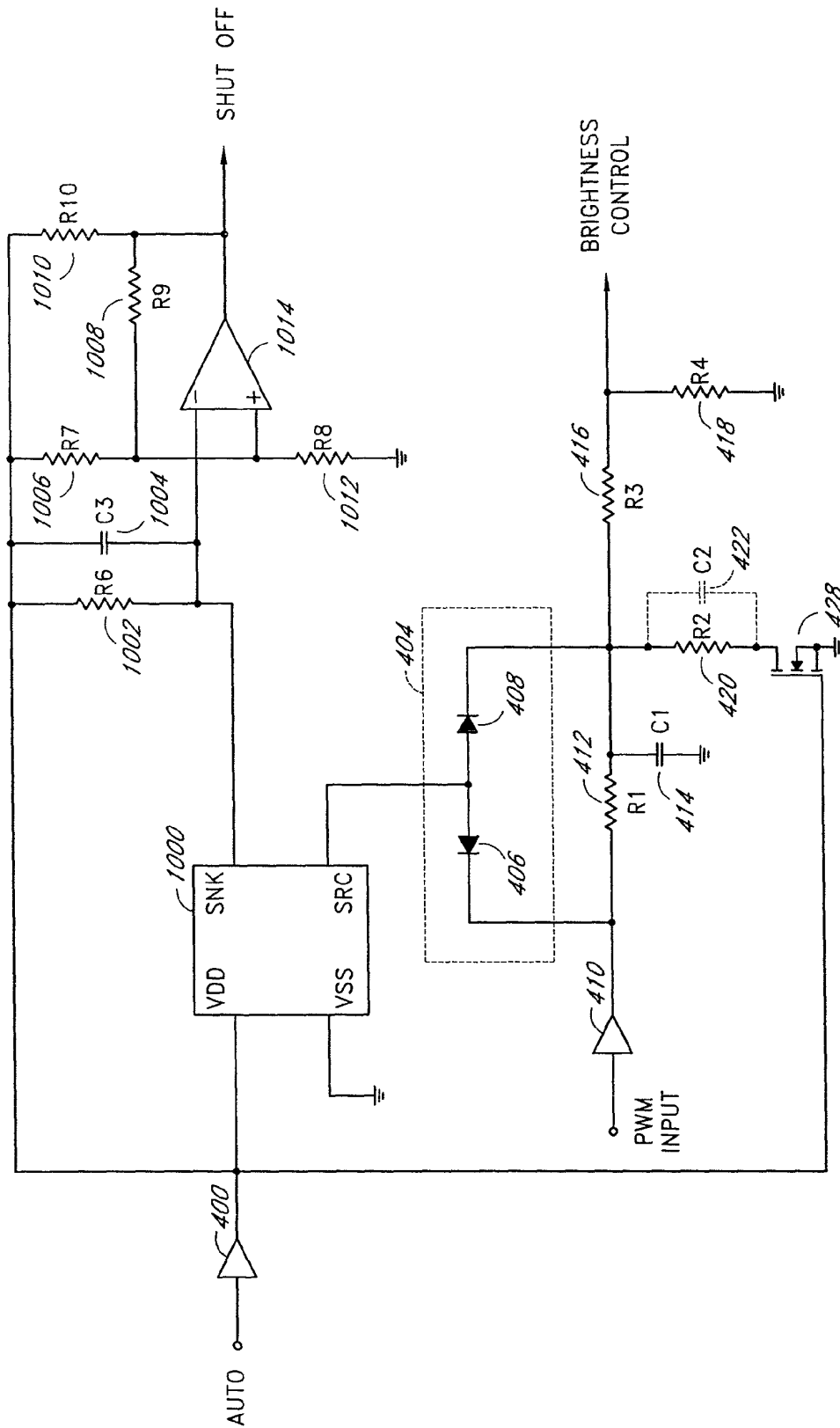


FIG. 10



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METHOD AND APPARATUS TO CONTROL DISPLAY BRIGHTNESS WITH AMBIENT LIGHT CORRECTION

CLAIM FOR PRIORITY

This application is a continuation of U.S. patent application Ser. No. 11/023,295, filed on Dec. 27, 2004 and entitled "Method and Apparatus to Control Display Brightness with Ambient Light Correction," which claims the benefit of priority under 35 U.S.C. § 119(e) of U.S. Provisional Application No. 60/543,094, filed on Feb. 9, 2004, and entitled "Information Display with Ambient Light Correction," each of which is hereby incorporated by reference herein in their entirety.

BACKGROUND OF THE INVENTION

1. Field of the Invention

The present invention relates to brightness control in a visual information display system, and more particularly relates to adjusting the brightness level to compensate for changes in ambient lighting.

2. Description of the Related Art

Backlight is needed to illuminate a screen to make a visible display in liquid crystal display (LCD) applications. The ability to read the display is hampered under conditions of high ambient room lighting. Ambient lighting reflects off the surface of the LCD and adds a bias to the light produced by the LCD, which reduces the display contrast to give the LCD a washed-out appearance. The condition can be improved by increasing the brightness of the backlight for the LCD, thereby making the light provided by the LCD brighter in comparison to the reflected light off the LCD surface. Thus, the backlight should be adjusted to be brighter for high ambient lighting conditions and less bright for low ambient lighting conditions to maintain consistent perceived brightness.

In battery operated systems, such as notebook computers, it is advantageous to reduce power consumption and extend the run time on a battery between charges. One method of reducing power consumption, and therefore extending battery run time, is to reduce the backlight brightness of a LCD under low ambient lighting conditions. The backlight can operate at a lower brightness level for low ambient lighting conditions because light reflections caused by the ambient light are lower and produce less of a washed-out effect. It is also advantageous to turn down the backlight under low ambient lighting conditions to extend the life of light sources in the backlight system. Typically, the light sources have a longer lifetime between failures if they run at lower brightness levels.

In some LCD applications, an ambient light sensor is used in a closed-loop configuration to adjust the backlight level in response to the ambient light level. These systems usually do not take into account user preferences. These systems are crude in implementation and do not adapt well to user preferences which may vary under various levels of eye fatigue.

SUMMARY OF THE INVENTION

In one embodiment, the present invention is a light sensor control system that provides the capability for a fully automatic and fully adaptable method of adjusting display brightness in response to varying ambient lighting conditions in combination with various user preferences. For example, the mathematical product of a light sensor output and a user selectable brightness control can be used to vary backlight intensity in LCD applications. Using the product of the light

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sensor output and the user selectable brightness control advantageously offers noticeable user dimming in bright ambient levels. Power is conserved by automatically dimming the backlight in low ambient light levels. The user control feature allows the user to select a dimming contour which works in conjunction with a visible light sensor.

In one embodiment, software algorithm can be used to multiply the light sensor output with the user selectable brightness control. In another embodiment, analog or mixed-signal circuits can be used to perform the multiplication. Digitizing the light sensor output or digital processing to combine the user brightness contour selection with the level of ambient lighting is advantageously not needed. The light sensor control system can be autonomous to a processor for a display device (e.g., a main processor in a computer system of a LCD device).

In one embodiment, a backlight system with selective ambient light correction allows a user to switch between a manual brightness adjustment mode and an automatic brightness adjustment mode. In the manual mode, the user's selected brightness preference determines the backlight brightness, and the user dims or increases the intensity of the backlight as the room ambient light changes. In the automatic mode, the user adjusts the brightness level of the LCD to a desired level, and as the ambient light changes, the backlight automatically adjusts to make the LCD brightness appear to stay consistent at substantially the same perceived level. The automatic mode provides better comfort for the user, saves power under low ambient lighting conditions, and prevents premature aging of light sources in the backlight system.

The mathematical product of a light sensor output and a user selectable brightness control can be similarly used to vary brightness in cathode ray tube (CRT) displays, plasma displays, organic light emitting diode (OLED) displays, and other visual information display systems that do not use backlight for display illumination. In one embodiment, a brightness control circuit with ambient light correction includes a visible light sensor that outputs a sensor current signal in proportion to the level of ambient light, a dimming control input determined by a user, and a multiplier circuit that generates a brightness control signal based on a mathematical product of the sensor current signal and the dimming control input. The brightness control signal is provided to a display driver (e.g., an inverter) to adjust brightness levels of one or more light sources, such as cold cathode fluorescent lamps (CCFLs) or light emitting diodes (LEDs) in a backlight system. The brightness control circuit with ambient light correction advantageously improves ergonomics by maintaining consistent brightness as perceived by the human eye. The brightness control circuit with ambient light correction also reduces power consumption to extend battery life and reduces stress on the light sources to extend product life at low ambient light levels.

In various embodiments, the brightness control circuit further includes combinations of a dark level bias circuit, an overdrive clamp circuit, or an automatic shutdown circuit. The dark level bias circuit maintains the brightness control signal above a predetermined level when the ambient light level decreases to approximately zero. Thus, the dark level bias circuit ensures a predefined (or minimum) brightness in total ambient darkness. The overdrive clamp circuit limits the brightness control signal to be less than a predetermined level. In one embodiment, the overdrive clamp circuit facilitates compliance with input ranges for the display driver. The automatic shutdown circuit turns off the light sources when the ambient light is greater than a predefined level. For example, the automatic shutdown circuit saves power by turn-

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ing off auxiliary light sources when ambient light is sufficient to illuminate a transreflective display.

The visible light sensor changes (e.g., increases or decreases) linearly with the level of ambient light and advantageously has a spectral response that approximates the spectral response of a human eye. In one embodiment, the visible light sensor uses an array of PIN diodes on a single substrate to detect ambient light. For example, an initial current in proportion to the ambient light level is generated from taking the difference between outputs of a full spectrum PIN diode and an infrared sensitive PIN diode. The initial current is amplified by a series of current mirrors to be the sensor current signal. In one embodiment, the initial current is filtered (or bandwidth limited) before amplification to adjust the response time of the visible light sensor. For example, a capacitor can be used to filter the initial current and to slow down the response time of the visible light sensor such that the sensor current signal remain substantially unchanged during transient variations in the ambient light (e.g., when objects pass in front of the display).

In one embodiment, the dimming control input is a pulse-width-modulation (PWM) logic signal that a user can vary from 0%-100% duty cycle. The PWM logic signal can be generated by a microprocessor based on user preference. In one embodiment, the dimming control input indicates user preference using a direct current (DC) signal. The DC signal and a saw-tooth ramp signal can be provided to a comparator to generate an equivalent PWM logic signal. The user preference can also be provided in other forms, such as a potentiometer setting or a digital signal (e.g., a binary word).

As discussed above, the multiplier circuit generates the brightness control signal using a multiplying function to correct for ambient light variations. The brightness control signal takes into account both user preference and ambient light conditions. The brightness control signal is based on the mathematical product of respective signals representing the user preference and the ambient light level.

In one embodiment, the multiplier circuit includes a pair of current steering diodes to multiply the sensor current signal with a PWM logic signal representative of the user preference. The sensor current signal is provided to a network of resistors when the PWM logic signal is high and is directed away from the network of resistors when the PWM logic signal is low. The network of resistors generates and scales the brightness control signal for the backlight driver. At least one capacitor is coupled to the network of resistors and configured as a low pass filter for the brightness control signal.

In one embodiment in which the user preference is indicated by a potentiometer setting, the visible light sensor output drives a potentiometer to perform the mathematical product function. For example, an isolation diode is coupled between the visible light sensor output and the potentiometer. The potentiometer conducts a portion of the sensor current signal to generate the brightness control signal. A network of resistors can also be connected to the potentiometer to scale the brightness control signal. An optional output capacitor can be configured as a low pass filter for the brightness control signal.

In one embodiment in which the user preference is indicated by a digital word, the multiplier circuit includes a digital-to-analog converter (DAC) to receive the digital word and output a corresponding analog voltage as the brightness control signal. The sensor current signal from the visible light sensor is used to generate a reference voltage for the DAC. For example, an isolation diode is coupled between the visible light sensor and a network of resistors. The network of resistors conducts the sensor current signal to generate the refer-

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ence voltage. An optional capacitor is coupled to the network of resistors as a low pass filter for the reference voltage. The DAC multiplies the reference voltage by the input digital word to generate the analog voltage output.

For the purposes of summarizing the invention, certain aspects, advantages and novel features of the invention have been described herein. It is to be understood that not necessarily all such advantages may be achieved in accordance with any particular embodiment of the invention. Thus, the invention may be embodied or carried out in a manner that achieves or optimizes one advantage or group of advantages as taught herein without necessarily achieving other advantages as may be taught or suggested herein.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a block diagram of one embodiment of a brightness control circuit with ambient light correction.

FIG. 2 is a block diagram of another embodiment of a brightness control circuit with ambient light correction.

FIG. 3 illustrates brightness control signals as a function of ambient light levels for different user settings.

FIG. 4 is a schematic diagram of one embodiment of a brightness control circuit with a multiplier circuit to combine a light sensor output with a user adjustable PWM logic signal.

FIG. 5 illustrates one embodiment of an ambient light sensor.

FIG. 6 illustrates one embodiment of an ambient light sensor with an adjustable response time.

FIG. 7 illustrates conversion of a direct current signal to a PWM logic signal.

FIG. 8 is a schematic diagram of one embodiment of a brightness control circuit with a multiplier circuit to combine a light sensor output with a user adjustable potentiometer.

FIG. 9 is a schematic diagram of one embodiment of a brightness control circuit with a multiplier circuit to combine a light sensor output with a user adjustable digital word.

FIG. 10 is a schematic diagram of one embodiment of a brightness control circuit with automatic shut down when ambient light is above a predetermined threshold.

DETAILED DESCRIPTION OF THE EMBODIMENTS

Embodiments of the present invention will be described hereinafter with reference to the drawings. FIG. 1 is a block diagram of one embodiment of a brightness control circuit with ambient light correction. A user input (DIMMING CONTROL) is multiplied by a sum of a dark level bias (DARK LEVEL BIAS) and a light sensor output (LIGHT SENSOR) to produce a brightness control signal (BRIGHTNESS CONTROL) for a display driver 112. In one configuration, the dark level bias and the light sensor output are adjusted by respective scalar circuits (k1, k2) 100, 102 before being added by a summing circuit 104. An output of the summing circuit 104 and the user input is provided to a multiplier circuit 106. An output of the multiplier circuit 106 can be adjusted by a third scalar circuit (k3) 108 to produce the brightness control signal. An overdrive clamp circuit 110 is coupled to the brightness control signal to limit its amplitude range at the input of the display driver 112.

The display driver 112 can be an inverter for fluorescent lamps or a LED driver that controls backlight illumination of LCDs in portable electronic devices (e.g., notebook computers, cell phones, etc.), automotive displays, electronic dashboards, television, and the like. The brightness control circuit with ambient light correction provides closed-loop adjust-

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ment of backlight brightness due to ambient light variations to maintain a desired LCD brightness as perceived by the human eye. The brightness control circuit advantageously reduces the backlight brightness under low ambient light conditions to improve efficiency. A visible light sensor detects the ambient light level and generates the corresponding light sensor output. The user input can come from processors in LCD devices. The brightness control circuit with ambient light correction advantageously operates independently of the processors in the LCD devices. The display driver 112 can also be used to control display brightness in CRT displays, plasma displays, OLED displays, and other visual information display systems that do not use backlight for display illumination.

FIG. 2 is a block diagram of another embodiment of a brightness control circuit with ambient light correction. A light sensor output (LIGHT SENSOR) is adjusted by a scalar circuit (k2) 102 and then provided to a multiplier circuit 106. A user input (DIMMING CONTROL) is also provided to the multiplier circuit 106. The multiplier circuit 106 outputs a signal that is the product of the user input and scaled light sensor output. A summing circuit 104 adds the product to a dark level bias (DARK LEVEL BIAS) that has been adjusted by scalar circuit (k1) 100. An output of the summing circuit 104 is adjusted by scalar circuit (k3) 108 to generate a brightness control signal (BRIGHTNESS CONTROL) for a display driver 112. An overdrive clamp 110 is coupled to the brightness control signal to limit its amplitude range at the input of the display driver 112.

The brightness control circuits shown in both FIGS. 1 and 2 automatically adjust the level of the brightness control signal in response to varying ambient light. The configuration of FIG. 2 provides a predefined level of brightness in substantially total ambient darkness and independent of the user input. For example, the output of the multiplier circuit 106, in both FIGS. 1 and 2, is substantially zero if the user input is about zero. The multiplier circuit 106 can be implemented using software algorithm or analog/mixed-signal circuitry. In FIG. 2, the scaled dark level bias is added to the output of the multiplier circuit 106 to provide the predefined level of brightness in this case. This feature may be desired to prevent a user from using the brightness control circuit to turn off a visual information display system.

FIG. 3 illustrates brightness control signals as a function of ambient light levels for different user settings in accordance with the brightness control circuit of FIG. 1. For example, ambient light levels are indicated in units of lux (or lumens/square meter) on a horizontal axis (or x-axis) in increasing order. Brightness control signal levels are indicated as a percentage of a predefined (or full-scale) level on a vertical axis (or y-axis).

Graph 300 shows a first brightness control signal as a function of ambient light level given a first user setting (e.g., 100% duty cycle PWM dimming input). Graph 302 shows a second brightness control signal as a function of ambient light level given a second user setting (e.g., 80% duty cycle PWM dimming input). Graph 304 shows a third brightness control signal as a function of ambient light level given a third user setting (e.g., 60% duty cycle PWM dimming input). Graph 306 shows a fourth brightness control signal as a function of ambient light level given a fourth user setting (e.g., 40% duty cycle PWM dimming input). Graph 308 shows a fifth brightness control signal as a function of ambient light level given a fifth user setting (e.g., 20% duty cycle PWM dimming input). Finally, graph 310 shows a sixth brightness control signal as a function of ambient light level given a sixth user setting (e.g., 0% duty cycle PWM dimming input).

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Graph 310 lies substantially on top of the horizontal axis in accordance with the sixth user setting corresponding to turning off the visual information display system. For the other user settings (or user adjustable dimming levels), the brightness control signal increases (or decreases) with increasing (or decreasing) ambient light levels. The rate of increase (or decrease) depends on the user setting. For example, higher user settings cause the associated brightness control signals to increase faster as a function of ambient light level. The brightness control signal near zero lux is a function of a dark bias level and also depends on the user setting. In one embodiment, the brightness control signal initially increases linearly with increasing ambient light level and reaches saturation (or 100% of full-scale) after a predetermined ambient light level. The saturation point is different for each user setting. For example, the brightness control signal begins to saturate at about 200 lux for the first user setting, at about 250 lux for the second user setting, and at about 350 lux for the third user setting. The brightness control circuit can be designed for different saturation points and dark bias levels.

FIG. 4 is a schematic diagram of one embodiment of a brightness control circuit with a multiplier circuit to combine a light sensor output with a user adjustable PWM logic signal (PWMINPUT). For example, the user adjustable PWM logic signal varies in duty cycle from 0% for minimum user-defined brightness to 100% for maximum user-defined brightness. A microprocessor can generate the user adjustable PWM logic signal based on user input which can be adjusted in response to various levels of eye fatigue for optimal viewing comfort. In one embodiment, the user adjustable PWM logic signal is provided to an input buffer circuit 410.

The brightness control circuit includes a visible light sensor 402, a pair of current-steering diodes 404, a network of resistors (R1, R2, R3, R4) 412, 420, 416, 418, a filter capacitor (C1) 414, and an optional smoothing capacitor (C2) 422. In one embodiment, the brightness control circuit selectively operates in a manual mode or an auto mode. The manual mode excludes the visible light sensor 402, while the auto mode includes the visible light sensor 402 for automatic adjustment of display brightness as ambient light changes. An enable signal (AUTO) selects between the two modes. For example, the enable signal is provided to a buffer circuit 400. An output of the buffer circuit 400 is coupled to an input (A) of the visible light sensor 402. The output of the buffer circuit 400 is also provided to a gate terminal of a metal-oxide-semiconductor field-effect-transistor (MOSFET) switch 428. The MOSFET switch 428 is an n-type transistor with a source terminal coupled to ground and a drain terminal coupled to a first terminal of the second resistor (R2) 420.

The pair of current-steering diodes 404 includes a first diode 406 and a second diode 408 with commonly connected anodes that are coupled to an output (B) of the visible light sensor 402. The first resistor (R1) 412 is coupled between the respective cathodes of the first diode 406 and the second diode 408. An output of the input buffer circuit 410 is coupled to the cathode of the first diode 406. The filter capacitor 414 is coupled between the cathode of the second diode 408 and ground. A second terminal of the second resistor 420 is coupled to the cathode of the second diode 408. The optional smoothing capacitor 422 is coupled across the second resistor 420. The third and fourth resistors 416, 418 are connected in series between the cathode of the second diode 408 and ground. The commonly connected terminals of the third and fourth resistors 416, 418 provide a brightness control signal to an input (BRITE) of a display driver (e.g., a backlight driver) 424. In one embodiment, the display driver 424 delivers

power to one or more light sources (e.g., fluorescent lamps) **426** coupled across its outputs.

In the auto mode, the enable signal is logic high and the buffer circuit **400** also outputs logic high (or VCC) to turn on the visible light sensor **402** and the MOSFET switch **428**. The visible light sensor **402** outputs a sensor current signal in proportion to sensed ambient light level. The sensor current signal and the user adjustable PWM logic signal are multiplied using the pair of current-steering diodes **404**. For example, when the user adjustable PWM logic signal is high, the sensor current signal flows through the second diode **408** towards the brightness control signal (or output). When the user adjustable PWM logic signal is low, the sensor current signal flows through the first diode **406** away from the output or into the input buffer circuit **410**. The equation for the brightness control signal (BCS1) in the auto mode is:

$$BCS1 = \text{duty cycle} \times \left[\left(\frac{VCC \times R2 \times R4}{[(R1 + R2) \times (R3 + R4)] + (R1 \times R2)} \right) + \left(\frac{ISRC \times R1 \times R2 \times R4}{[(R1 + R2) \times (R3 + R4)] + (R1 \times R2)} \right) \right]$$

The term “duty cycle” corresponds to the duty cycle of the user adjustable PWM logic signal. The term “VCC” corresponds to the logic high output from the input buffer circuit **410**. The term “ISRC” corresponds to the sensor current signal. The first major term within the brackets corresponds to a scaled dark bias level of the brightness control signal in total ambient darkness. The second major term within the brackets introduces the effect of the visible light sensor **402**. The network of resistors **412**, **420** **416**, **418** helps to provide the dark bias level and to scale the product of the sensor current signal and the user adjustable PWM logic signal.

For example, the first resistor **412** serves to direct some current from the input buffer circuit **410** to the output in total ambient darkness. The second, third, and fourth resistors **420**, **416**, **418** provide attenuation to scale the brightness control signal to be compatible with the operating range of the display driver **424**. The filter capacitor **414** and the optional smoothing capacitor **422** slow down the response time of the back-light brightness control circuit to reduce flicker typically associated with indoor lighting sources. In the auto mode, the brightness control signal clamps when the voltage at the cathode of the second diode **408** approaches the compliance voltage of the visible light sensor **402** plus a small voltage drop across the second diode **408**.

In the manual mode, the enable signal is logic low. Consequently, the visible light sensor **402** and the MOSFET switch **428** are off. The pair of current-steering diodes **404** isolates the visible light sensor **402** from the rest of the circuit. The off-state of the MOSFET switch **428** removes the influence of the second resistor **420** and the optional smoothing capacitor **422**. The equation for the brightness control signal (BCS2) in the manual mode is:

$$BCS2 = VCC \times \text{duty cycle} \times \frac{R4}{(R1 + R3 + R4)}$$

In the manual mode, the filter capacitor **414** filters the user adjustable PWM logic signal. The brightness control circuit has an option of having two filter time constants, one for the manual mode and one for the auto mode. The time constant for the manual mode is determined by the filter capacitor **414** in combination with the first, third and fourth resistors **412**,

416, **418**. The node impedance presented to the filter capacitor **414** is typically high during the manual mode. The time constant for the auto mode can be determined by the optional smoothing capacitor **422**, which is typically larger in value, to slow down the response of the visible light sensor **402**. The node impedance presented to the optional smoothing capacitor **422** is typically low. The optional smoothing capacitor **422** may be eliminated if the visible light sensor **402** is independently bandwidth limited.

FIG. 5 illustrates one embodiment of an ambient light sensor. The ambient light sensor includes a light detector **500**, a first transistor **502**, a second transistor **504** and an additional current amplifier circuit **506**. The light detector **500** generates an initial current in response to sensed ambient light. The first transistor **502** and the second transistor **504** are configured as current mirrors to respectively conduct and duplicate the initial current. The second transistor **504** can also provide amplification of the duplicated initial current. The additional current amplifier circuit **506** provides further amplification of the current conducted by the second transistor **504** to generate a sensor current signal at an output of the ambient light sensor.

For example, the light detector (e.g., a photodiode or an array of PIN diodes) **500** is coupled between an input (or power) terminal (VDD) and a drain terminal of the first transistor **502**. The first transistor **502** is an n-type MOSFET connected in a diode configuration with a source terminal coupled to ground. The first transistor **502** conducts the initial current generated by the light detector **500**. The second transistor **504** is also an n-type MOSFET with a source terminal coupled to ground. Gate terminals of the first and second transistors **502**, **504** are commonly connected. Thus, the second transistor **504** conducts a second current that follows the initial current and is scaled by the geometric ratios between the first and second transistors **502**, **504**. The additional current amplifier circuit **506** is coupled to a drain terminal of the second transistor **504** to provide amplification (e.g., by additional current mirror circuits) of the second current. The output of the additional current amplifier circuit **506** (i.e., the sensor current signal) is effectively a multiple of the initial current generated by the light detector **500**.

FIG. 6 illustrates one embodiment of an ambient light sensor with an adjustable response time. The ambient light sensor of FIG. 6 is substantially similar to the ambient light sensor of FIG. 5 and further includes a program capacitor **508** and source degeneration resistors **510**, **512**. For example, the source degeneration resistors **510**, **512** are inserted between ground and the respective source terminals of the first and second transistors **502**, **504**. The program capacitor **508** is coupled between the source terminal of the first transistor **502** and ground.

The program capacitor **508** filters the initial current generated by the light detector **500** and advantageously provides the ability to adjust the response time of the ambient light sensor (e.g., by changing the value of the program capacitor **508**). In a closed loop system, such as automatic brightness control for a computer display or television, it may be desirable to slow down the response time of the ambient light sensor so that the automatic brightness control is insensitive to passing objects (e.g., moving hands or a person walking by). A relatively slower response by the ambient light sensor allows the automatic brightness control to transition between levels slowly so that changes are not distracting to the viewer.

The response time of the ambient light sensor can also be slowed down by other circuitry downstream of the ambient light sensor, such as the optional smoothing capacitor **422** in the brightness control circuit of FIG. 4. The brightness control circuit of FIG. 4 has two filter time constants, one for the

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manual mode in which the visible light sensor **402** is not used and another for the auto mode which uses the visible light sensor **402**. In one embodiment, the optional smoothing capacitor **422** is included in the auto mode to slow down the response time of the brightness control circuit to accommodate the visible light sensor **402**.

The optional smoothing capacitor **422** may have an unintentional side effect of slowing down the response time of the brightness control circuit to the user adjustable PWM logic signal. This unintentional side effect is eliminated by using the program capacitor **508** to separately and independently slow down the response time of the ambient light sensor to a desired level. The optional smoothing capacitor **422** can be eliminated from the brightness control circuit which then has one filter time constant for both the auto and manual modes.

The program capacitor **508** can be coupled to different nodes in the ambient light sensor to slow down response time. However, it is advantageous to filter (or limit the bandwidth of) the initial current rather than an amplified version of the initial current because the size and value of the program capacitor **508** can be smaller and lower, therefore more cost-efficient.

FIG. 7 illustrates conversion of a DC signal (DC DIMMING INPUT) to a PWM logic signal (PWM INPUT). The DC signal (or DC dimming interface) is used in some backlight systems to indicate user dimming preference. In one embodiment, a comparator **700** can be used to convert the DC signal to the PWM logic signal used in the brightness control circuit of FIG. 4. For example, the DC signal is provided to a non-inverting input of the comparator **700**. A periodic sawtooth signal (SAWTOOTH RAMP) is provided to an inverting input of the comparator **700**. The periodic sawtooth signal can be generated using a **C555** timer (not shown). The comparator **700** outputs a PWM signal with a duty cycle determined by the level of the DC signal. Other configurations to convert the DC signal to the PWM logic signal are also possible.

FIG. 8 is a schematic diagram of one embodiment of a brightness control circuit with a multiplier circuit to combine a light sensor output with a user adjustable potentiometer (**R3**) **812**. Some display systems use the potentiometer **812** for user dimming control. The brightness control circuit configures a visible light sensor **802** to drive the potentiometer **812** with a current signal proportional to ambient light to generate a brightness control signal (BRIGHTNESS CONTROL) at its output.

For example, the potentiometer **812** has a first terminal coupled to ground and a second terminal coupled to a supply voltage (VCC) via a first resistor (**R1**) **810**. A second resistor (**R2**) **808** in series with a p-type MOSFET switch **806** are coupled in parallel with the first resistor **810**. The second terminal of the potentiometer **812** is also coupled to an output of visible light sensor **802** via an isolation diode **804**. The isolation diode **804** has an anode coupled to the output of the visible light sensor **802** and a cathode coupled to the second terminal of the potentiometer **812**. A fourth resistor (**R4**) **814** is coupled between the second terminal of the potentiometer **812** and the output of the brightness control circuit. A capacitor (Cout) **816** is coupled between the output of the brightness control circuit and ground.

In one embodiment, the brightness control circuit of FIG. 8 selectively operates in an auto mode or a manual mode. An enable signal (AUTO) indicates the selection of operating mode. The enable signal is provided to a buffer circuit **800**, and an output of the buffer circuit **800** is coupled to an input of the visible light sensor **802** and a gate terminal of the p-type MOSFET switch **806**. When the enable signal is logic high to

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indicate operation in the auto mode, the buffer circuit **800** turns on the visible light sensor **802** and disables (or turns off) the p-type MOSFET switch **806**. Turning off the p-type MOSFET switch **806** effectively removes the second resistor **808** from the circuit. The equation for the brightness control signal (BCS3) at the output of the brightness control circuit during auto mode operation is:

$$BCS3 = \left[VCC \times \frac{R3}{(R1 + R3)} \right] + \left[ISRC \times \frac{(R1 \times R3)}{(R1 + R3)} \right]$$

The first major term in brackets of the above equation corresponds to the brightness control signal in total ambient darkness. The second major term in brackets introduces the effect of the visible light sensor **802**. The maximum range for the brightness control signal in the auto mode is determined by the compliance voltage of the visible light sensor **802**.

The enable signal is logic low to indicate operation in the manual mode, and the buffer circuit **800** turns off the visible light sensor **802** and turns on the p-type MOSFET switch **806**. Turning on the p-type MOSFET switch **806** effectively couples the second resistor **808** in parallel with the first resistor **810**. The equation for the brightness control signal (BCS4) at the output of the brightness control circuit during manual mode operation is:

$$BCS4 = VCC \times \frac{R3 \times (R1 + R2)}{(R1 \times R2) + (R1 \times R3) + (R2 \times R3)}$$

FIG. 9 is a schematic diagram of one embodiment of a brightness control circuit with a multiplier circuit to combine a light sensor output with a user adjustable digital word. Some display systems use a DAC **918** for dimming control. A binary input (bn . . . b1) is used to indicate user dimming preference. The DAC **918** generates an analog voltage (Vout) corresponding to the binary input. The analog voltage is the brightness control signal at an output of the brightness control circuit. In one embodiment, a voltage clamp circuit **920** is coupled to the output brightness control circuit to limit the range of the brightness control signal.

The value of the analog voltage also depends on a reference voltage (Vref) of the DAC **918**. In one embodiment, the reference voltage is generated using a sensor current signal from a visible light sensor **902** that senses ambient light. For example, the visible light sensor **902** drives a network of resistors (**R1**, **R2**, **R3**) **906**, **902**, **912** through an isolation diode **904**. An output of the visible light sensor **902** is coupled to an anode of the isolation diode **904**. The first resistor (**R1**) **906** is coupled between a supply voltage (VCC) and a cathode of the isolation diode **904**. The second resistor (**R2**) **908** is coupled in series with a semiconductor switch **910** between the cathode of the isolation diode **904** and ground. The third resistor (**R3**) **912** is coupled between the cathode of the isolation diode **904** and ground. An optional capacitor **914** is coupled in parallel with the third resistor **912** to provide filtering. An optional buffer circuit **916** is coupled between the cathode of the isolation diode **904** and the reference voltage input of the DAC **918**.

The brightness control circuit of FIG. 9 can be configured for manual mode operation with the visible light sensor **902** disabled or for auto mode operation with the visible light sensor **902** enabled. An enable signal (AUTO) is provided to a buffer circuit **900** to make the selection between auto and manual modes. An output of the buffer circuit **900** is provided

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to an input of the visible light sensor **902** and to a gate terminal of the semiconductor switch **910**.

When the enable signal is logic high to select auto mode operation, the visible light sensor **902** is active and the semiconductor switch **910** is on to effectively couple the second resistor **908** in parallel with the third resistor **912**. In the auto mode, the equation for the brightness control signal (BCS5) at the output of the DAC **918** is:

BCS5 =

$$\text{binary \% fullscale} \times \left[\frac{[VCC \times (R2 \times R3)] + [ISRC \times R1 \times R2 \times R3]}{(R1 \times R2) + (R1 \times R3) + (R2 \times R3)} \right]$$

When the enable signal is logic low to select manual mode operation, the visible light sensor **902** is disabled and the semiconductor switch **910** is off to effectively remove the second resistor **908** from the circuit. In the manual mode, the equation for the brightness control signal (BCS6) at the output of the DAC **918** is:

$$BCS6 = \text{binary \% fullscale} \times VCC \times \frac{R3}{(R1 + R3)}$$

FIG. **10** is a schematic diagram of one embodiment of a brightness control circuit with automatic shut down when ambient light is above a predetermined threshold. When lighting transfective displays, it may be preferred to shut off auxiliary light sources (e.g., backlight or frontlight) when ambient lighting is sufficient to illuminate the display. In addition to generating the brightness control signal (BRIGHTNESS CONTROL), the brightness control circuit of FIG. **10** includes a shut down signal (SHUT OFF) to disable the backlight or the frontlight when the ambient light level is above the predetermined threshold.

The brightness control circuit of FIG. **10** advantageously uses a visible light sensor **1000** with two current source outputs that produce currents that are proportional to the sensed ambient light. The two current source outputs include a sourcing current (SRC) and a sinking current (SNK). The sourcing current is used to generate the brightness control signal. By way of example, the portion of the circuit generating the brightness control signal is substantially similar to the brightness control circuit shown in FIG. **4** and is not further discussed.

The sinking current is used to generate the shut down signal. In one embodiment, a comparator **1014** generates the shut down signal. A resistor (R6) **1002** is coupled between a selective supply voltage and the sinking current output of the visible light sensor **1000** to generate a comparison voltage for an inverting input of the comparator **1014**. A low pass filter capacitor (C3) **1004** is coupled in parallel with the resistor **1002** to slow down the reaction time of the sinking current output to avoid triggering on 60 hertz light fluctuations. A resistor (R7) **1006** coupled in series with a resistor (R8) **1012** between the selective supply voltage and ground generates a threshold voltage for a non-inverting input of the comparator **1014**. A feedback resistor (R9) coupled between an output of the comparator **1014** and the non-inverting input of the comparator **1014** provides hysteresis for the comparator **1014**. A pull-up resistor (R10) is coupled between the selective supply voltage and the output of the comparator **1014**. The selective supply voltage may be provided by the output of the buffer circuit **400** which also enables the visible light sensor **1000**.

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When the ambient level is relatively low, the sinking current is relatively small and the voltage drop across the resistor **1002** conducting the sinking current is correspondingly small. The comparison voltage at the inverting input of the comparator **1014** is greater than the threshold voltage at the non-inverting input of the comparator, and the output of the comparator **1014** is low. When the ambient level is relatively high, the sinking current is relatively large and the voltage drop across the resistor **1002** is also large. The comparison voltage at the inverting input of the comparator **1014** becomes less than the threshold voltage and the comparator **1014** outputs logic high to activate the shut down signal. Other configurations may be used to generate the shut down signal based on the sensed ambient light level.

While certain embodiments of the inventions have been described, these embodiments have been presented by way of example only, and are not intended to limit the scope of the inventions. Indeed, the novel methods and systems described herein may be embodied in a variety of other forms; furthermore, various omissions, substitutions and changes in the form of the methods and systems described herein may be made without departing from the spirit of the inventions. The accompanying claims and their equivalents are intended to cover such forms or modifications as would fall within the scope and spirit of the inventions.

What is claimed is:

1. A brightness control circuit with selective ambient light correction comprising:

- a first input configured to receive a user signal indicative of a user selectable brightness setting;
- a light sensor configured to sense ambient light and to output a sensing signal indicative of the ambient light level;
- a multiplier configured to selectively generate a combined signal based on both the user signal and the sensing signal; and
- a dark level bias configured to adjust the combined signal to generate a brightness control signal that is used to control a brightness level of a visible display such that the brightness control signal is maintained above a predetermined level when the ambient light level decreases to approximately zero.

2. The brightness control circuit of claim 1, wherein the dark level bias is provided to the multiplier such that the amount of adjustment to the combined signal is dependent on the user selectable brightness setting.

3. The brightness control circuit of claim 2, wherein the multiplier multiplies a sum of the user signal and the sensing signal by the dark level bias to generate an output signal corresponding to the brightness control signal.

4. The brightness control circuit of claim 1, wherein the dark level bias is added to the combined signal such that the amount of adjustment to the combined signal is independent of the user selectable brightness setting.

5. The brightness control circuit of claim 4, wherein the dark level bias is added to an output of the multiplier.

6. The brightness control circuit of claim 1, further comprising an overdrive clamp circuit coupled to the brightness control signal to limit its amplitude to a predefined range.

7. The brightness control circuit of claim 1, wherein the brightness control signal is provided to a display driver to control backlight illumination of a liquid crystal display.

8. The brightness control circuit of claim 7, further comprising a shut down circuit configured to turn off the display driver when the sensing signal is above a predetermined threshold.

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9. The brightness control circuit of claim 1, further comprising a second input configured to receive a selection signal to selectively operate the brightness control circuit in an auto mode or a manual mode, wherein the selection signal enables the light sensor in the auto mode and disables the light sensor in the manual mode.

10. The brightness control circuit of claim 1, wherein the multiplier is implemented with a pair of current-steering diodes having commonly connected anodes coupled to the sensing signal and respective cathodes coupled to the user signal and a network of resistors to generate the brightness control signal.

11. The brightness control circuit of claim 1, wherein the user signal corresponds to a setting of a user adjustable potentiometer, and the multiplier is implemented with an isolation diode having an anode coupled to the sensing signal and a cathode coupled to the user adjustable potentiometer and a network of resistors to generate the brightness control signal.

12. The brightness control circuit of claim 1, wherein the user signal corresponds to a digital word, and the multiplier is implemented with a digital-to-analog converter configured to receive the digital word and a reference signal determined by the sensing signal to generate the brightness control signal.

13. The brightness control circuit of claim 1, wherein the light sensor comprises a full spectrum PIN diode, an infrared sensitive PIN diode, and an amplifier configured to generate the sensing signal based on a difference between an output of the full spectrum PIN diode and an output of the infrared sensitive PIN diode.

14. The brightness control circuit of claim 13, wherein the light sensor further comprises a low pass filter to reduce sensitivity to transient variations of ambient light.

15. A method to selectively provide ambient light correction, said method comprising:
receiving a user input signal indicative of a user selectable brightness setting;

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selectively multiplying the input signal with a sense signal to generate a combined signal, wherein the sense signal indicates an ambient light level; and

adjusting the combined signal with a dark level bias to generate a brightness control signal for controlling brightness of a visible display such that the brightness control signal is maintained above a predetermined level when the ambient light level decreases to approximately zero.

16. The method of claim 15, wherein the step of selectively multiplying the input signal with the sense signal is performed by a software algorithm, an analog circuit, or a mixed-signal circuit.

17. The method of claim 15, wherein the dark level bias is added to the sense signal before selective multiplication such that the amount of adjustment to the combined signal is dependent on the input signal.

18. The method of claim 15, wherein the dark level bias is added to the combined signal after selective multiplication such that the amount of adjustment to the combined signal is independent of the input signal and the sense signal.

19. A brightness control circuit comprising:

means for receiving an input signal indicative of a user selectable brightness setting;

means for sensing ambient light to generate a sense signal indicative of the ambient light level;

means for multiplying the input signal with the sense signal to generate a combined signal; and

means for adjusting the combined signal with a dark level bias to generate a brightness control signal that is maintained above a minimum level when the ambient light level decreases to approximately zero.

20. The brightness control circuit of claim 19, further comprising means for selectively operating in a manual mode or an auto mode, wherein the means for sensing ambient light is enabled in the auto mode and disabled in the manual mode.

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