



US010656301B2

(12) **United States Patent**
Donderici et al.

(10) **Patent No.: US 10,656,301 B2**
(45) **Date of Patent: May 19, 2020**

(54) **REDUCING EFFECTS OF CONDUCTIVE MUD ON SINGLE-WELL RANGING**

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(*) Notice: Subject to any disclaimer, the term of this
patent is extended or adjusted under 35
U.S.C. 154(b) by 423 days.

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(21) Appl. No.: **15/538,291**

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(22) PCT Filed: **Jun. 20, 2016**

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(86) PCT No.: **PCT/US2016/038410**

§ 371 (c)(1),

(2) Date: **Jun. 21, 2017**

(Continued)

(87) PCT Pub. No.: **WO2017/222500**

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PCT Pub. Date: **Dec. 28, 2017**

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(65) **Prior Publication Data**

US 2018/0210107 A1 Jul. 26, 2018

(51) **Int. Cl.**

G01V 3/20 (2006.01)

E21B 43/24 (2006.01)

(Continued)

(52) **U.S. Cl.**

CPC **G01V 3/20** (2013.01); **E21B 43/2406**
(2013.01); **E21B 47/02216** (2013.01); **E21B**
47/122 (2013.01); **E21B 47/124** (2013.01)

(58) **Field of Classification Search**

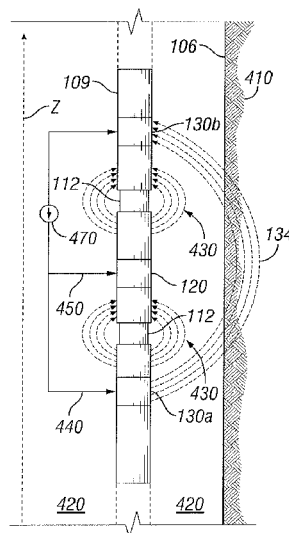
CPC . G01V 3/20; E21B 43/2406; E21B 47/02216;
E21B 47/122; E21B 47/124

See application file for complete search history.

(57) **ABSTRACT**

An example downhole tool for determining ranging param-
eters involves placing a guard electrode between a survey
electrode and a return electrode where the survey electrode
and the return electrode are separated by a gap subs. A fixed,
predictable, and stable path for the survey current is formed
that is independent of the conductivity of the mud or
conductive targets resulting in a formation current that may
be used to estimate the direction, orientation or distance of
a conductive target. The formation current is then a stable
current that excites a conductive target in the same way
regardless of the conductivity of the mud so as to obtain a
mud-independent reference signal in single-well ranging.

20 Claims, 7 Drawing Sheets



- (51) **Int. Cl.**
E21B 47/022 (2012.01)
E21B 47/12 (2012.01)

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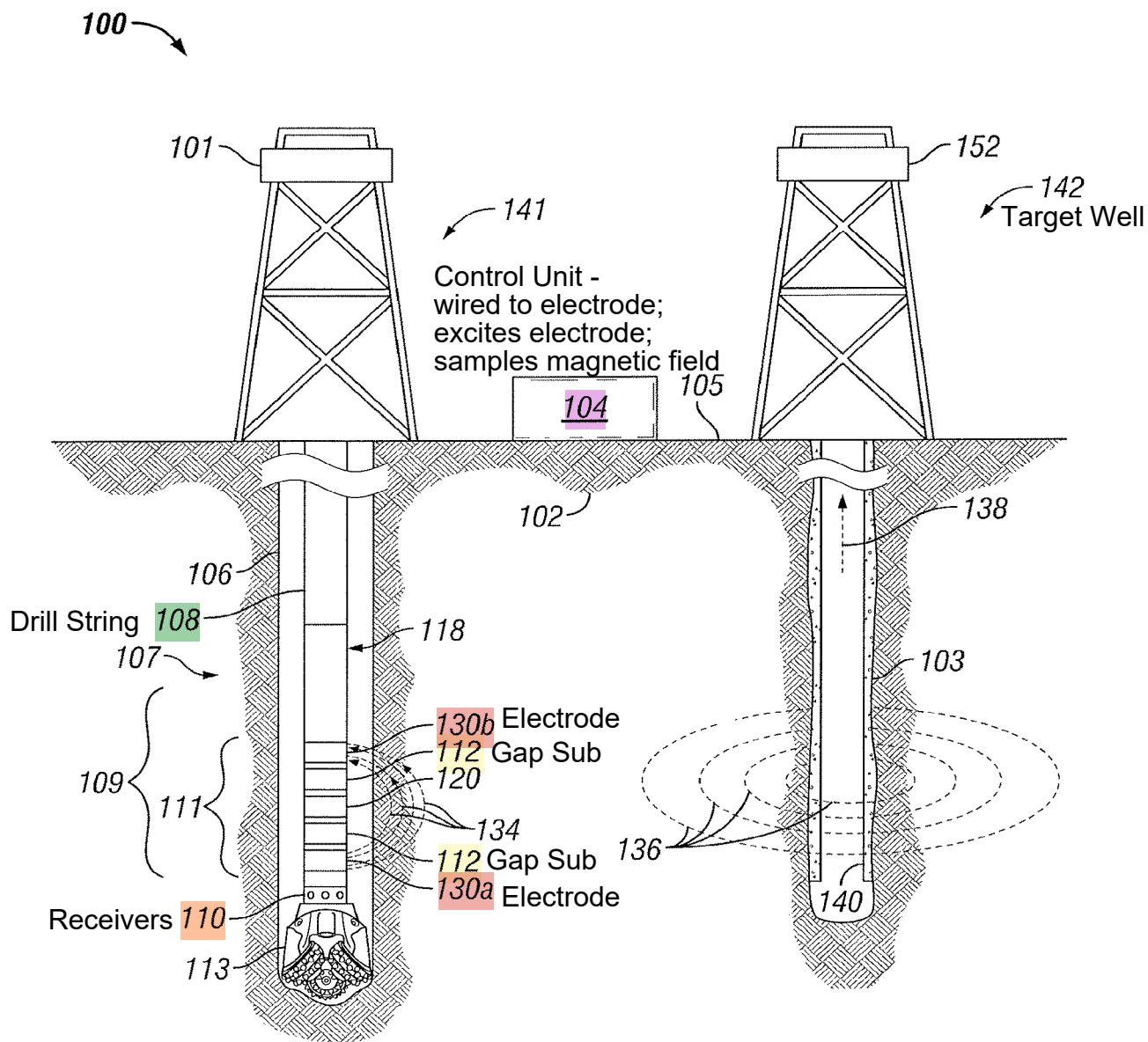
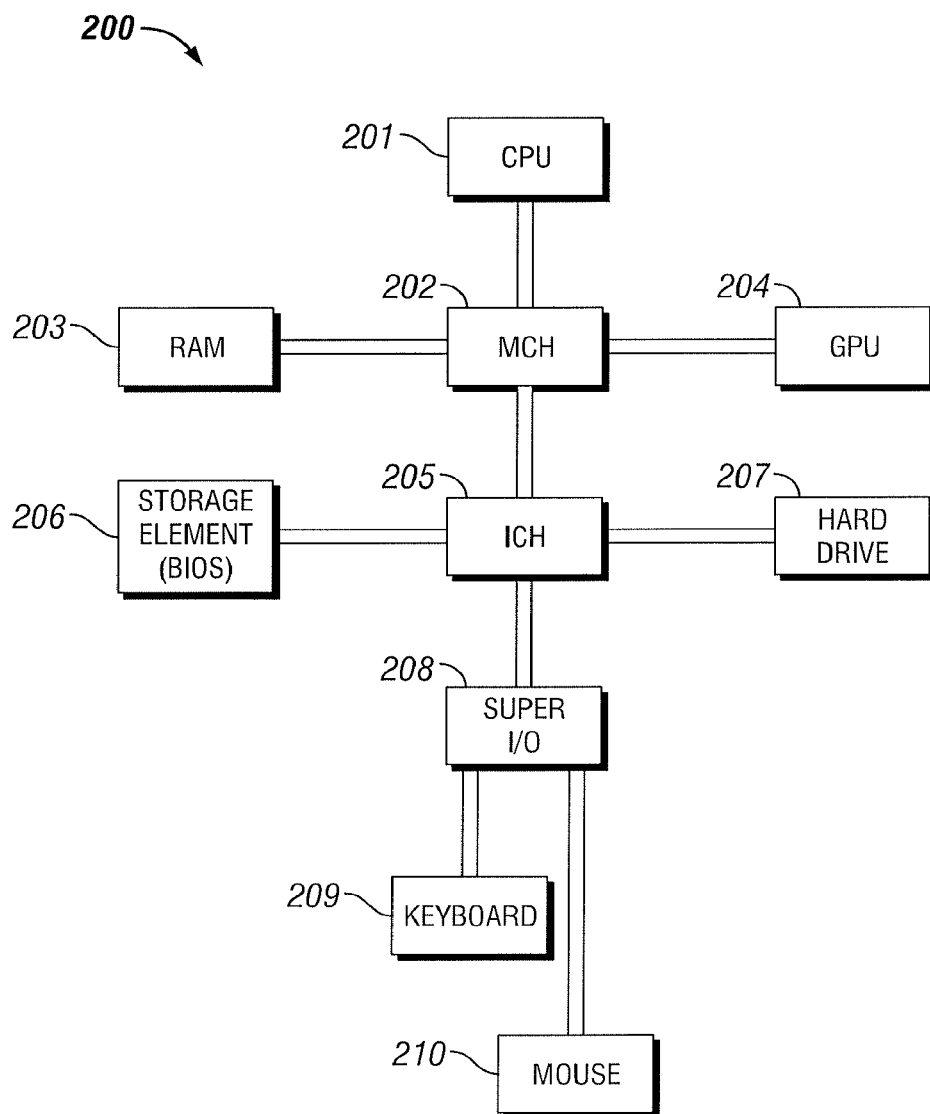


FIG. 1

**FIG. 2**

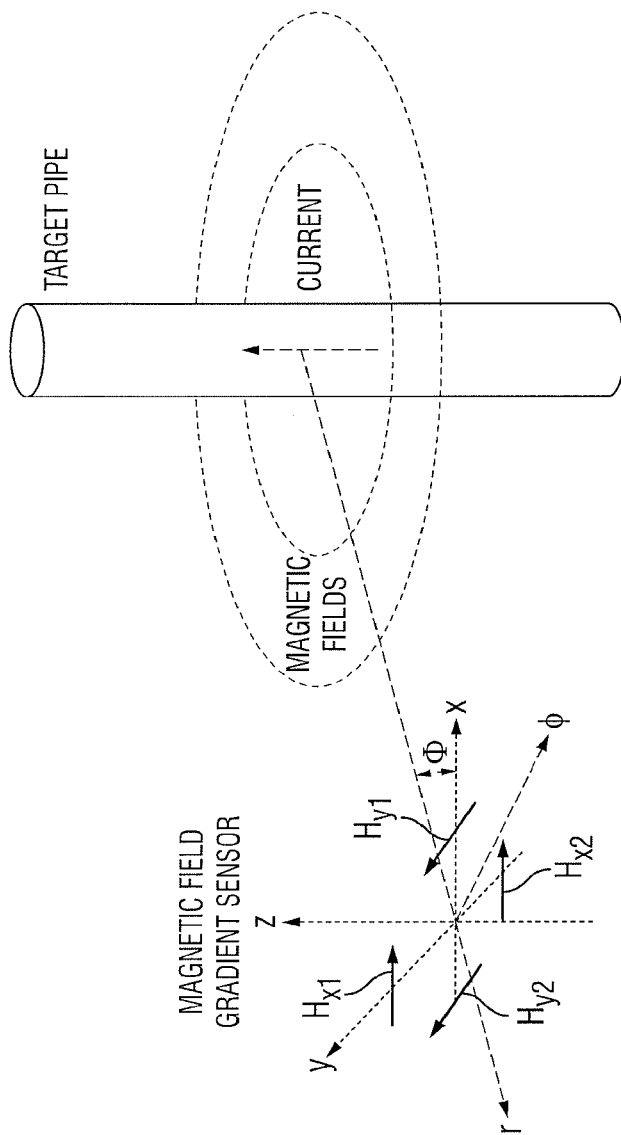


FIG. 3

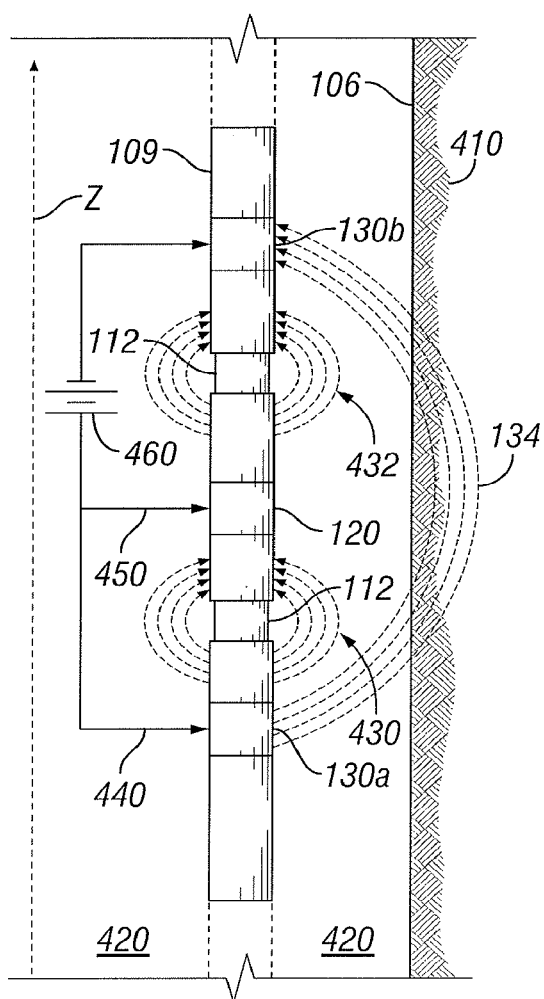


FIG. 4A

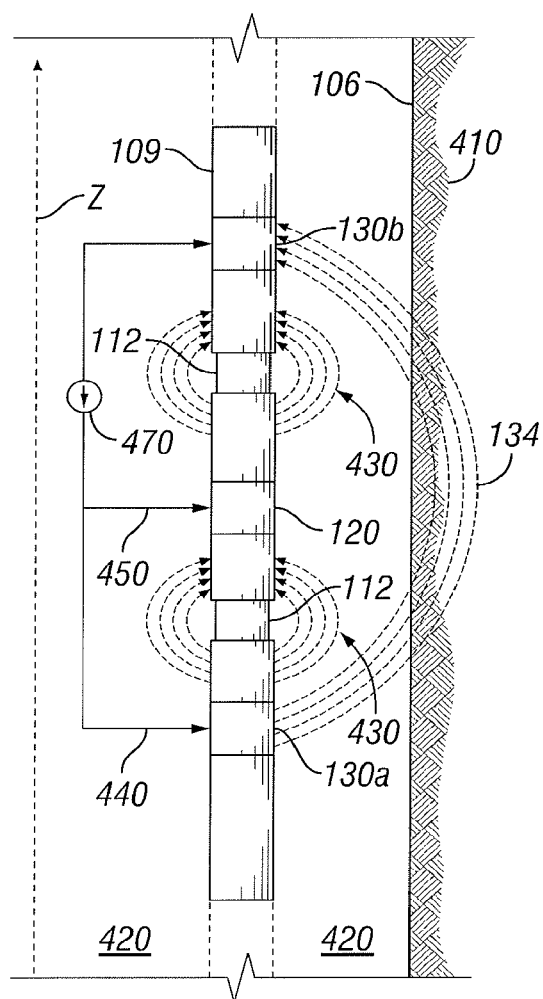


FIG. 4B

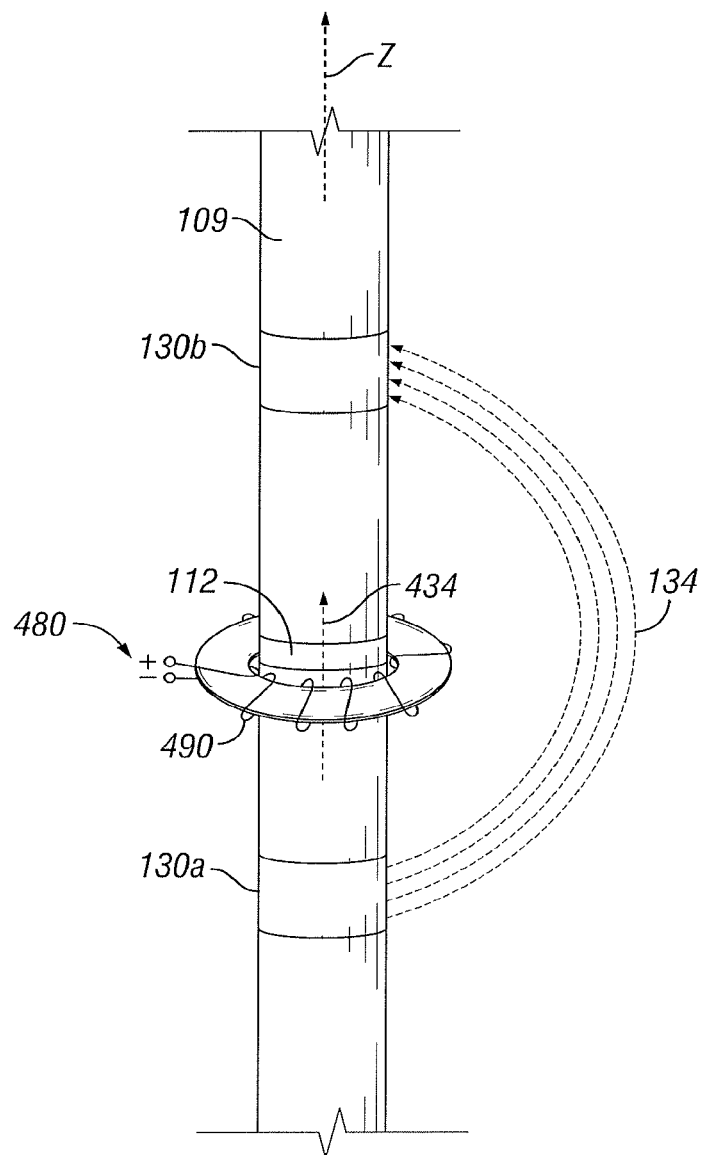
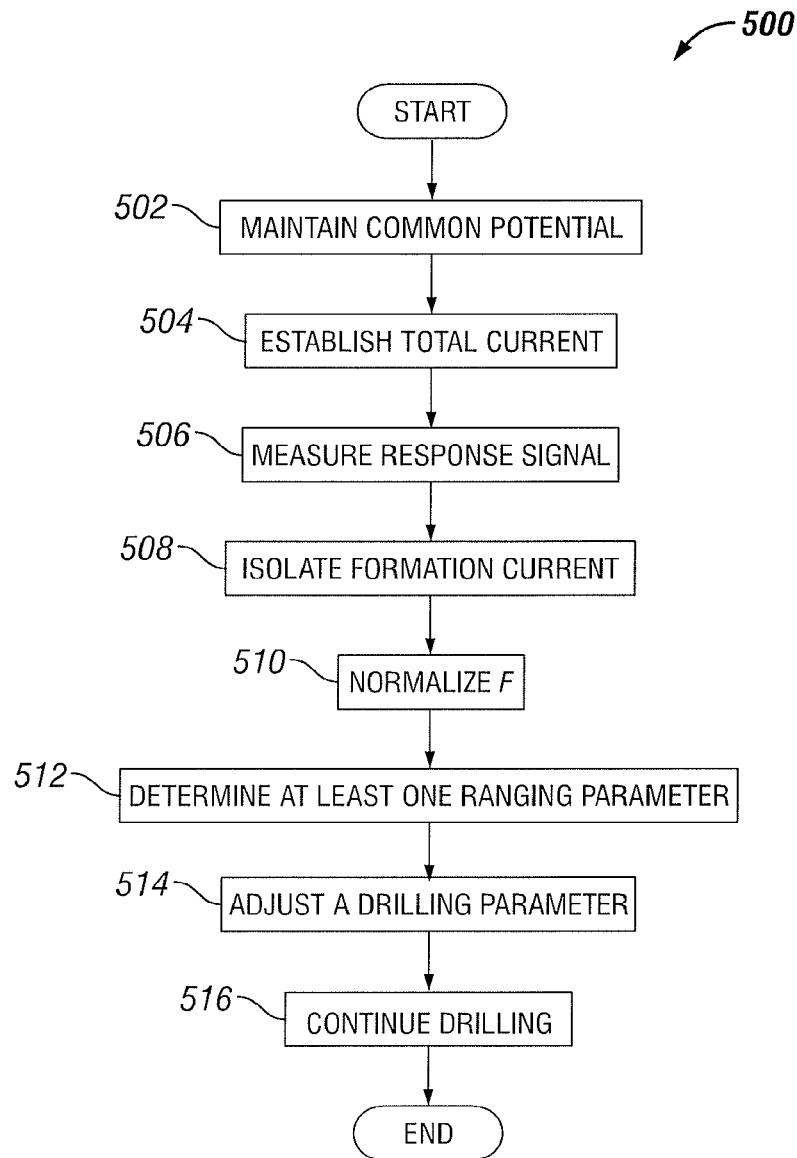
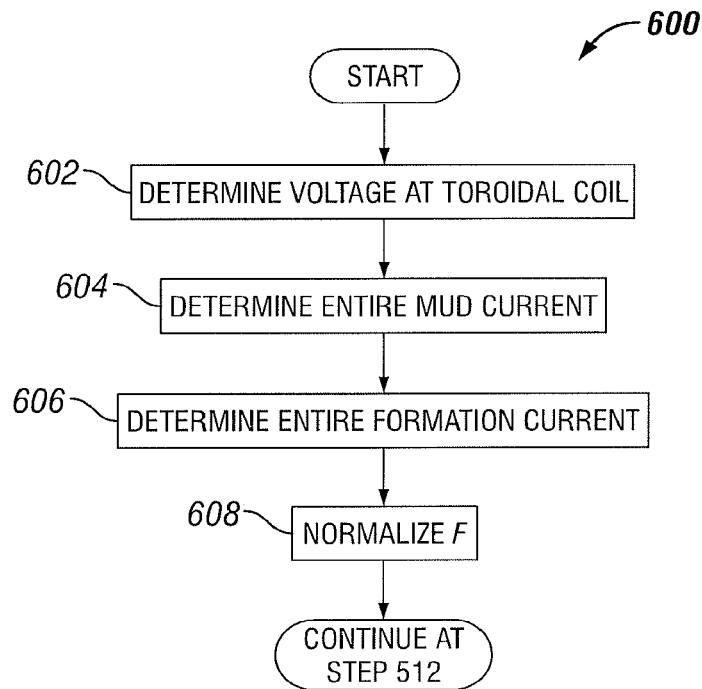
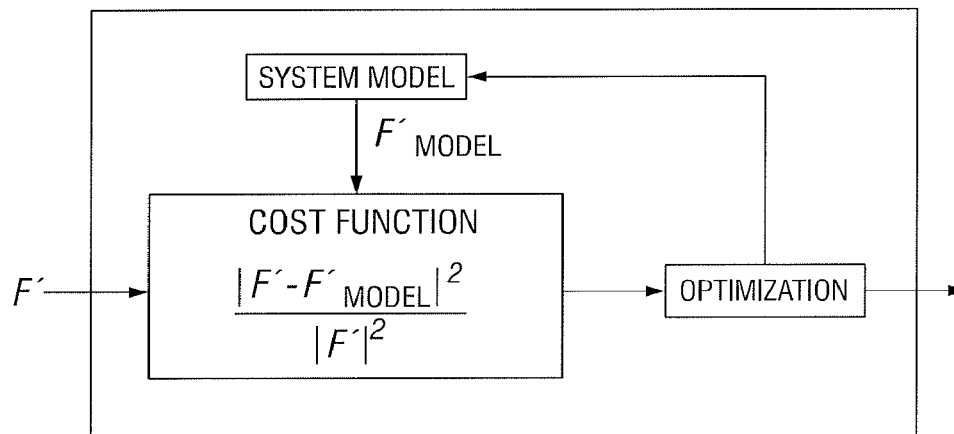


FIG. 4C

**FIG. 5**

**FIG. 6****FIG. 7**

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REDUCING EFFECTS OF CONDUCTIVE MUD ON SINGLE-WELL RANGING

CROSS-REFERENCE TO RELATED APPLICATION

The present application is a U.S. National Stage Application of International Application No. PCT/US2016/038410 filed Jun. 20, 2016, which is incorporated herein by reference in its entirety for all purposes.

BACKGROUND

The present disclosure relates generally to well logging operations and, more particularly, to an improvement in making ranging measurements using a galvanic tool by reducing the effects of conductive mud.

Hydrocarbons, such as oil and gas, are commonly obtained from subterranean formations that may be located onshore or offshore. The development of subterranean operations and the processes involved in removing hydrocarbons from a subterranean formation are complex. Typically, subterranean operations involve a number of different steps such as, for example, drilling a wellbore at a desired well site, treating the wellbore to optimize production of hydrocarbons, and performing the necessary steps to produce and process the hydrocarbons from the subterranean formation.

Existing well drilling operations require information on formation characteristics to aid in drilling decisions. Numerous measurement techniques are used, including logging while drilling (LWD), measuring while drilling (MWD), electromagnetic (EM) ranging applications, and wireline. One such measurement technique includes the use of a galvanic tool to take ranging measurements of the surrounding formation. Galvanic tools may include one or more electrodes through which current is injected into and returned from the formation to generate the ranging measurements. During typical operation current should ideally only flow between selected ones of the electrodes. In practice, however, "leakage current" may run through other ones of the electrodes. This may reduce the accuracy of the resulting ranging measurements.

FIGURES

Some specific exemplary embodiments of the disclosure may be understood by referring, in part, to the following description and the accompanying drawings.

FIG. 1 is a diagram showing an illustrative logging while drilling environment, according to aspects of the present disclosure.

FIG. 2 is a diagram of an example information handling system, according to aspects of the present disclosure.

FIG. 3 is a diagram illustrating example gradient measurement components in relation to a target object and the magnetic fields produced by currents on the target object.

FIGS. 4A, 4B, and 4C are diagrams illustrating a cross-sectional view of a downhole system for galvanic excitation, according to aspects of the present disclosure.

FIG. 5 is a flow diagram of an example ranging method, according to aspects of the present disclosure.

FIG. 6 is a flow diagram of an example ranging method, according to aspects of the present disclosure.

FIG. 7 is a diagram illustrating an inversion model, according to aspects of the present disclosure.

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While embodiments of this disclosure have been depicted and described and are defined by reference to exemplary embodiments of the disclosure, such references do not imply a limitation on the disclosure, and no such limitation is to be inferred. The subject matter disclosed is capable of considerable modification, alteration, and equivalents in form and function, as will occur to those skilled in the pertinent art and having the benefit of this disclosure. The depicted and described embodiments of this disclosure are examples only, and not exhaustive of the scope of the disclosure.

Throughout this disclosure, a reference numeral followed by an alphabetical character refers to a specific instance of an element and the reference numeral alone refers to the element generically or collectively. Thus, as an example (not shown in the drawings), widget "12a" refers to an instance of a widget class, which may be referred to collectively as widgets "12" and any one of which may be referred to generically as a widget "12". In the figures and the description, like numerals are intended to represent like elements.

DETAILED DESCRIPTION

The present disclosure relates generally to well drilling operations and, more particularly, to obtaining an improved ranging measurement using a galvanic tool.

For purposes of this disclosure, an information handling system may include any instrumentality or aggregate of instrumentalities operable to compute, classify, process, transmit, receive, retrieve, originate, switch, store, display, manifest, detect, record, reproduce, handle, or utilize any form of information, intelligence, or data for business, scientific, control, or other purposes. For example, an information handling system may be a personal computer, a network storage device, or any other suitable device and may vary in size, shape, performance, functionality, and price. The information handling system may include random access memory (RAM), one or more processing resources such as a central processing unit (CPU) or hardware or software control logic, ROM, and/or other types of nonvolatile memory. Additional components of the information handling system may include one or more disk drives, one or more network ports for communication with external devices as well as various input and output (I/O) devices, such as a keyboard, a mouse, and a video display. The information handling system may also include one or more buses operable to transmit communications between the various hardware components. The information handling system may also include one or more interface units capable of transmitting one or more signals to a controller, actuator, or like device.

For the purposes of this disclosure, computer-readable media may include any instrumentality or aggregation of instrumentalities that may retain data and/or instructions for a period of time. Computer-readable media may include, for example, without limitation, storage media such as a direct access storage device (for example, a hard disk drive or floppy disk drive), a sequential access storage device (for example, a tape disk drive), compact disk, CD-ROM, DVD, RAM, ROM, electrically erasable programmable read-only memory (EEPROM), and/or flash memory; as well as communications media such as wires, optical fibers, microwaves, radio waves, and other electromagnetic and/or optical carriers; and/or any combination of the foregoing.

Illustrative embodiments of the present disclosure are described in detail herein. In the interest of clarity, not all features of an actual implementation may be described in this specification. It will of course be appreciated that in the

development of any such actual embodiment, numerous implementation specific decisions are made to achieve the specific implementation goals, which will vary from one implementation to another. Moreover, it will be appreciated that such a development effort might be complex and time-consuming, but would nevertheless be a routine undertaking for those of ordinary skill in the art having the benefit of the present disclosure.

To facilitate a better understanding of the present disclosure, the following examples of certain embodiments are given. In no way should the following examples be read to limit, or define, the scope of the disclosure. Embodiments of the present disclosure may be applicable to horizontal, vertical, deviated, or otherwise nonlinear wellbores in any type of subterranean formation. Embodiments may be applicable to injection wells as well as production wells, including hydrocarbon wells. Embodiments may be implemented using a tool that is made suitable for testing, retrieval and sampling along sections of the formation. Embodiments may be implemented with tools that, for example, may be conveyed through a flow passage in tubular string or using a wireline, slickline, coiled tubing, downhole robot or the like.

The terms “couple” or “couples” as used herein are intended to mean either an indirect or a direct connection. Thus, if a first device couples to a second device, that connection may be through a direct connection or through an indirect mechanical or electrical connection via other devices and connections. Similarly, the term “communicatively coupled” as used herein is intended to mean either a direct or an indirect communication connection. Such connection may be a wired or wireless connection such as, for example, Ethernet or local area network (LAN). Such wired and wireless connections are well known to those of ordinary skill in the art and will therefore not be discussed in detail herein. Thus, if a first device communicatively couples to a second device, that connection may be through a direct connection, or through an indirect communication connection via other devices and connections.

Modern petroleum drilling and production operations demand information relating to parameters and conditions downhole. Several methods exist for downhole information collection, including LWD and MWD, and wireline. In LWD, data is typically collected during the drilling process, thereby avoiding any need to remove the drilling assembly to insert a wireline logging tool. LWD consequently allows the driller to make accurate real-time modifications or corrections to optimize performance while minimizing down time. MWD is the term for measuring conditions downhole concerning the movement and location of the drilling assembly while the drilling continues. LWD concentrates more on formation parameter measurement. While distinctions between MWD and LWD may exist, the terms MWD and LWD often are used interchangeably. For the purposes of this disclosure, the term LWD will be used with the understanding that this term encompasses both the collection of formation parameters and the collection of information relating to the movement and position of the drilling assembly.

The accuracy of resistivity measurements from galvanic tools may be improved by accounting for and/or minimizing leakage currents between the electrodes of a galvanic tool. As will be described in detail below, galvanic tool leakage currents may be accounted for in the resulting resistivity measurements by isolating the current that flows into the formation from the current excited at an electrode. In certain embodiments, the leakage currents that run through the

electrodes of the galvanic tool also are minimized by the introduction of a guard electrode between a gap sub and either of the electrodes of the galvanic tool.

FIG. 1 is a diagram illustrating an example drilling and ranging system environment **100**, according to aspects of the present disclosure. The environment **100** includes rig **101** at the surface **105** associated with a well **141** and positioned above borehole **106** within a subterranean formation **102**. Rig **101** may be coupled to a drilling assembly **107**, comprising drill string **108** and bottom hole assembly (BHA) **109**. The BHA **109** may comprise a drill bit **113** and a downhole tool **111**. The downhole tool **111** may be any type of downhole tool **111** including, but not limited to, a MWD, an LWD, ranging tool, sensors, a galvanic tool, etc. The downhole tool **111** may include similar functionality as and/or be incorporated in any other component including but not limited to a MWD, LWD, or galvanic tool. In certain embodiments, the drilling assembly **107** may be rotated by a top drive mechanism (not shown) to rotate the drill bit **113** and extend the borehole **106**. In certain other embodiments, a downhole motor (not shown), such as a mud motor, may be included to rotate the drill bit **113** and extend the borehole **106** without rotating the drilling assembly **107**. Although not depicted, in one or more embodiments, such as in an offshore drilling operation, the surface **105** may be separated from the rig **101** by a volume of water.

As used herein, a galvanic tool may comprise any tool, such as downhole tool **111**, with electrodes or a toroidal coil through which current is injected into a subterranean formation and a voltage response of the formation to the injected current is measured. As the bit extends the borehole **106** through the formation **102**, the downhole tool **111** may collect resistivity measurements relating to borehole **106**, the borehole **103** and the formation **102**. In certain embodiments, the orientation and position of the downhole tool **111** may be tracked using, for example, an azimuthal orientation indicator, which may include magnetometers, inclinometers, and/or accelerometers, though other sensor types such as gyroscopes may be used in some embodiments.

One or more ranging operations may require that a location of a conductive target be identified. In the embodiment shown, the conductive target comprises a target well **142** for a second borehole **103** associated with a rig **152**. The borehole **103** may comprise a casing **140** containing or composed of an electrically conductive member such as casing, liner or a drill string or any portion thereof that has had a blowout or that needs to be intersected, followed, tracked or avoided. In the embodiment shown, the borehole **103** includes an electrically conductive casing **140**. Identifying the location of the target well **142** with conductive casing **140** may comprise taking various measurements and determining a distance, direction or orientation of the target well **142**.

In certain embodiments, performing ranging measurements may include inducing an electromagnetic (EM) field within the second borehole **103** based, at least in part, on a formation current **134** injected into the formation **102**. In the embodiment shown, inducing a magnetic field within the borehole **103** comprises injecting a formation current **134** by exciting a survey electrode **130a** to induce current to flow into the formation **102** and return at return electrode **130b**. The source of the excitation may be a voltage or a current. Electrodes **130** may be components of the downhole tool **111**, BHA **109**, or any other downhole tool or component. Formation current **134** may be induced within the formation **102** by energizing the survey electrode **130a** of the drilling assembly **107** according to a control signal that specifies

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signal characteristics for the formation current **134**. The formation current **134** may comprise, for example, an alternating current electrical signal. The transmit electrode **130a** may be a button, a cylindrical or semi-cylindrical sheet electrode, or an electrode of any other type that has a metallic surface in contact with or in very close proximity of the borehole wall **106**. Part of the formation current **134** may be received and concentrated at the casing **140** within the conductive target (target well **142**), shown as current **138**, and the current **138** on the casing **140** may induce a magnetic field **136** in a radial direction from the direction of the flow of the current **138**. A magnetic field **136** created by the conductive target or casing **140** may be proportional to the current flowing into the formation.

The drilling assembly **107** or the downhole tool **111** may include a gap sub **112** that may allow for a dipole electric field to be created to aid in flowing or drawing current into the formation **102**. In any embodiment, the survey electrode **130a** may be located on the order of 10-200 feet from the return electrode **130b** or at any range greater, lesser, or in between. A guard electrode **120** may be placed between the survey electrode **130a** and the return electrode **130b** to further isolate the current flowing into the formation **102**.

In certain embodiments, a system control unit **104** may be positioned at the surface **105** as depicted in FIG. 1 and may be communicably or communicatively coupled to downhole elements including, but not limited to, drilling assembly **107**, telemetry system **118**, downhole tool **111**, and BHA **109**. In other embodiments, a system control unit **104** may be positioned below the surface **105** (not shown) and may communicate data to another system control unit **104** or any other system, for example, an information handling system, capable of receiving data from the system control unit **104**. For example, the system control unit **104** may be communicably coupled to the MWD apparatus **111**, electrodes **130**, drill bit **113**, or any other component through a telemetry system **118**. The telemetry system **118** may be incorporated into the BHA **109** or any other downhole tool or component of drilling assembly **107** and may comprise a mud pulse type telemetry system that transmits information between the surface system control unit **104** and downhole elements via pressure pulses in drilling mud. Although the system control unit **104** is positioned at the surface **105** in FIG. 1, certain processing, memory, and control elements may be positioned within the drilling assembly **107**. Additionally, various other communication schemes may be used to transmit communications to/from the system control unit **104**, including wireline configurations and wireless configurations.

In certain embodiments, the system control unit **104** may comprise an information handling system with at least a processor and a memory device coupled to the processor that contains a set of instructions that when executed cause the processor to perform certain actions. In any embodiment, the information handling system may include a non-transitory computer readable medium that stores one or more instructions where the one or more instructions when executed cause the processor to perform certain actions. As used herein, an information handling system may include any instrumentality or aggregate of instrumentalities operable to compute, classify, process, transmit, receive, retrieve, originate, switch, store, display, manifest, detect, record, reproduce, handle, or utilize any form of information, intelligence, or data for business, scientific, control, or other purposes. For example, an information handling system may be a computer terminal, a network storage device, or any other suitable device and may vary in size, shape, performance, functionality, and price. The information handling

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system may include random access memory (RAM), one or more processing resources such as a central processing unit (CPU) or hardware or software control logic, read only memory (ROM), and/or other types of nonvolatile memory. Additional components of the information handling system may include one or more disk drives, one or more network ports for communication with external devices as well as various input and output (I/O) devices, such as a keyboard, a mouse, and a video display. The information handling system may also include one or more buses operable to transmit communications between the various hardware components.

The formation current **134** may be injected into the formation **102** by excitation of the survey electrode **130a**. In certain embodiments, the system control unit **104** may excite the survey electrode **130a** by sending a command downhole to the downhole tool **111** or a controller (not shown) associated with the downhole tool **111**. The command(s) may cause the downhole tool **111** to excite the survey electrode **130a**. In other embodiments, the survey electrode **130a** is excited by a downhole source located at or associated with the downhole tool **111**. In one or more embodiments the source of excitation may be located downhole or at the surface **105**.

In certain embodiments, the signal characteristics of the formation current **134** may be based at least in part on at least one downhole characteristics within the borehole **106** and formation **102**, including a noise level within the formation **102**; a frequency transfer function of the survey electrode **130a**, the return electrode **130b**, the formation **102**; and a frequency response of the conductive target. The noise level within the formation **102** may be measured downhole using electromagnetic or acoustic receivers coupled to the drilling assembly, for example. The frequency transfer function and the frequency response of the target borehole **103** may be determined based on various mathematical models, or may be extrapolated from previous ranging measurements.

In certain embodiments, the system control unit **104** may further send commands to a receiver, for example, receiver **110**, to cause any one or more receivers **110** to measure the induced magnetic field **136** on the second borehole **103**. The receiver **110** may be a magnetometer, a collection of magnetometers, a solenoidal coil wrapped around the downhole tool **111** (for example, with a tilt between 0 degrees and 45 degrees), a solenoidal coil placed on the side of the downhole tool **111**, or a collection of solenoidal coils. Like the survey electrode **130a**, the receiver **110** may be coupled to a downhole controller, and the commands from the system control unit **104** may control, for example, when the measurements are taken. In certain embodiments, the system control unit **104** may determine and set a sampling rate of the induced magnetic field **136**, as will be described below. Additionally, measurements taken by the receiver **110** may be transmitted to the system control unit **104** via the telemetry system **118**. The control unit **104** may determine a distance, orientation and direction to the conductive target (for example, target well **142** or casing **140** of borehole **103**) in the embodiment shown, based at least in part on the measurement of the induced magnetic field **136**. For example, the system control unit **104** may use geometric algorithms to determine the distance, orientation and direction of the second borehole **103** relative to the borehole **106**.

FIG. 2 is a diagram illustrating an example information handling system **200**, according to aspects of the present disclosure. The system control unit **104** may take a form similar to the information handling system **200**. A processor

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or central processing unit (CPU) **201** of the information handling system **200** is communicatively coupled to a memory controller hub or north bridge **202**. The processor **201** may include, for example a microprocessor, microcontroller, digital signal processor (DSP), application specific integrated circuit (ASIC), or any other digital or analog circuitry configured to interpret and/or execute program instructions and/or process data. Processor **201** may be configured to interpret and/or execute program instructions or other data retrieved and stored in any memory such as memory **203** or hard drive **207**. Program instructions or other data may constitute portions of a software or application for carrying out one or more methods described herein. Memory **203** may include read-only memory (ROM), random access memory (RAM), solid state memory, or disk-based memory. Each memory module may include any system, device or apparatus configured to retain program instructions and/or data for a period of time (e.g., computer-readable non-transitory media). For example, instructions from a software or application may be retrieved and stored in memory **203** for execution by processor **201**.

Modifications, additions, or omissions may be made to FIG. 2 without departing from the scope of the present disclosure. For example, FIG. 2 shows a particular configuration of components of information handling system **200**. However, any suitable configurations of components may be used. For example, components of information handling system **200** may be implemented either as physical or logical components. Furthermore, in some embodiments, functionality associated with components of information handling system **200** may be implemented in special purpose circuits or components. In other embodiments, functionality associated with components of information handling system **200** may be implemented in configurable general purpose circuit or components. For example, components of information handling system **200** may be implemented by configured computer program instructions.

Memory controller hub **202** may include a memory controller for directing information to or from various system memory components within the information handling system **200**, such as memory **203**, storage element **206**, and hard drive **207**. The memory controller hub **202** may be coupled to memory **203** and a graphics processing unit **204**. Memory controller hub **202** may also be coupled to an I/O controller hub or south bridge **205**. I/O hub **205** is coupled to storage elements of the information handling system **200**, including a storage element **206**, which may comprise a flash ROM that includes a basic input/output system (BIOS) of the computer system. I/O hub **205** is also coupled to the hard drive **207** of the information handling system **200**. I/O hub **205** may also be coupled to a Super I/O chip **208**, which is itself coupled to several of the I/O ports of the computer system, including keyboard **209** and mouse **210**.

In certain embodiments, determining the distance, orientation and direction of a conductive target, for example, a second borehole **103**, relative to the borehole **106** may be accomplished using the magnetic fields received by the receiver **110**. In certain embodiments, the distance and direction determination may be achieved utilizing the relationship in Equation (1) between the casing current and the received magnetic fields.

$$\vec{H} = \frac{I}{2\pi r} \hat{\phi} \quad \text{Equation (1)}$$

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where $\vec{H}$ is the magnetic field vector, I is the current on the casing **140** (or a target pipe), r is the shortest distance between the receiver **110** and the casing **140**; and $\hat{\phi}$ is a vector that is perpendicular to both the z -axis of the receiver **110** and the shortest vector that connects the casing **140** to the receiver **110**. Although Equation (1) assumes constant casing current along the casing **140**, it can be extended to any current distribution by using the appropriate model.

In certain embodiments, the distance and direction of the second borehole **103** relative to the first borehole **106** may be determined using Equations (2) and (3), respectively.

$$r = \frac{I}{2\pi|\vec{H}|} \quad \text{and} \quad \text{Equation (2)}$$

$$\Phi = \text{angle}(\hat{x} \cdot \vec{H}, \hat{y} \cdot \vec{H}) + 90, \quad \text{Equation (3)}$$

where “ $\cdot$ ” is the vector inner-product operation. In certain instances, however, Equation (2) may be unreliable if a direct or accurate measurement of I is not possible.

When a direct or accurate measurement of I is difficult or impossible, magnetic field gradient measurement may be utilized for the direction and distance determinations. Spatial change in the magnetic field may be measured in a direction that has a substantial component in the radial (r -axis) direction as in Equation (4). For the gradient approach to work, the receiver **110** should be a collection of magnetometers or a collection of solenoidal coils.

$$\frac{\partial \vec{H}}{\partial r} = -\frac{I}{2\pi r^2} \hat{\phi}, \quad \text{Equation (4)}$$

where ∂ is the partial derivative. With this gradient measurement available in addition to an absolute measurement, the distance to the second borehole **103** may be calculated using Equation (5).

$$r = \frac{|\vec{H}|}{\left| \frac{\partial \vec{H}}{\partial r} \right|} \quad \text{Equation (5)}$$

In certain embodiments, the gradient field in Equation (5) may be realized in practice by utilizing finite difference of two magnetic field dipole measurements as shown below in Equation (6):

$$r = \frac{H_y}{\frac{H_y(x + \frac{\Delta x}{2}, y) - H_y(x - \frac{\Delta x}{2}, y)}{\Delta x}}, \quad \text{Equation (6)}$$

where H_y and the gradient measurement components are illustrated in the 4-dipole configuration of FIG. 3 in relation to a target casing **140** and the magnetic fields produced by currents on the casing **140**.

FIG. 4A, FIG. 4B, and FIG. 4C are cross-sections of example downhole systems for galvanic excitation. For purposes of this disclosure, the term BHA **109** will be used with the understanding that this term includes any other suitable downhole component of drilling assembly **107**. While BHA **109** is shown, the components may be included

as part of any component of the drilling assembly 107, for example, as downhole tool 111. Discussion regarding the BHA 109 may apply to any suitable downhole component. In particular embodiments, the geometry of the BHA 109 is cylindrically symmetric around the z axis and as such only the yz cross-section is illustrated. BHA 109 is disposed within borehole 106 where mud 420 flows between BHA 109 and a wall of the borehole 106. The total axial length of the BHA 109 may be orders of magnitude greater than the relative distances between the electrodes 130. The BHA 109 comprises at least two electrodes 130 (at least one survey electrode 130a and at least one return electrode 130b). The electrodes 130 may be located at any position along the BHA 109 and the orientation may be reversed, for example, survey electrode 130a may be located closer to the surface 105. The electrodes 130 may be direct contact with the body of the BHA 109. The BHA 109 may be metallic, with negligible resistivity compared to that of the mud 420 and the formation 102.

A gap sub 112 is located between the electrodes 130 (for example, survey electrode 130a and return electrode 130b) to electrically insulate two portions of the BHA 109 and to prevent shorting. The gap sub 112 may comprise insulating materials. As a result of excitation of the survey electrode 130a, a formation current 134 (I_{form}) flows through the formation 102 and reaches the return electrode 130b. As the mud 420 is typically present outside and/or inside the BHA 109, some current may cross a gap sub through the mud 420. A gap current provides no information regarding the conductive target (for example, target well 142) as a gap current does not flow into the formation 102. In some circumstances, a gap current may constitute a large portion of the total current (for example, survey current 440 (I_{survey})) delivered to the survey electrode 130a. As a gap current (such as return gap current (I_{gap1}) 432, survey gap current 430 (I_{gap2}), and toroidal gap current 434 (I_{gap3})) is not relevant to a determination of the distance, orientation or direction to a conductive target (for example, target well 142), more informative measurements may be acquired by subtracting gap currents from the survey current 440 prior to post-processing and inversion.

In particular embodiments, I_{gap1} 432 and I_{gap2} 430 are isolated by locating a guard electrode 120 between the survey electrode 130a and the return electrode 130b. The guard electrode 120 and the survey electrode 130a may be kept at the same potential by a source (for example, voltage source 460 and current source 470 in FIG. 4A and FIG. 4B, respectively). If the mud 420 is conductive, the guard current 450 may be essentially (or estimated to be) I_{gap1} 432 and the survey current 440 may be essentially (or estimated to be) the formation current 134. As the guard electrode 120 is kept at the same potential as the survey electrode 130a, I_{gap2} 430 approaches zero. As a result, the survey current 440 flows radially outward into the formation 102 as formation current 134, regardless of the resistivity of the mud 420. I_{gap1} 432 may be measured at a much greater value than zero when the mud 420 is conductive making the guard current 450 highly dependent on the resistivity of the mud 420. Since the survey current 440 is independent of the mud resistivity, the survey current 440 may be used as a normalization reference, resulting in the post-processing becoming independent of the mud resistivity as well. This normalization procedure of the present disclosure is discussed below with respect to the received signal F.

In FIG. 4C, a toroidal coil 490 is located along the BHA 109. The toroidal coil 490 is excited by a toroidal source 480. I_{gap3} 434 is directly measured using the toroidal coil

490 and removed from the induced total current to yield a formation current 134. The I_{gap3} 434 is measured using the toroidal coil 490 wrapped around the gap sub 112. The gap sub 112 and the toroidal coil 490 may be located anywhere along or within a groove of the BHA 109. The toroidal coil 490 may be located at, above or below the gap sub 112. In this way, the formation current 134 is isolated from the total current.

In particular embodiments, the survey electrode 130a, the return electrode 130b, and the guard electrode 120 are in direct electrical contact with the BHA 109 such that three elongated electrodes separated by two gap subs are essentially created. The sizes of the electrodes 130, the guard electrode 120 and the gap subs 112 as well as the distances between any one or more of them may be application specific. For example, the spacing between the survey electrode 130a and the return electrode 130b may be chosen to correspond to a value comparable to the desired depth of investigation of a ranging tool, for example, downhole tool 111. Depending on the ranging application (for example, well avoidance, well intervention, steam-assisted gravity drainage (SAGD)), the spacing may range from 2 meters to 100 meters.

In particular embodiments, the formation current 134 flows through a nearby conductive target such as conductive casing 140 of target well 142. The conductive target creates a secondary signal F (for example, magnetic field 136) somewhere in the downhole tool 111. This secondary signal F may be a current, a voltage, an electric field, or a magnetic field measured by a sensor on the downhole tool 111. To normalize F requires a reference signal which represents the strength of the excitation. The reference signal may be survey current 440 as it flows into the formation 102 and not across a gap sub 112. Using a total current (survey current 440 combined with guard current 450) increases complexity as the guard current 450 is sensitive to the resistivity of mud 420 which also introduces error into the inversion due to the possibility of an inaccurate mud resistivity.

FIG. 5 is a flow diagram of an example ranging method, according to aspects of the present disclosure. The ranging method of FIG. 5 may be implemented using any number of configurations for a downhole tool 111, for example, the BHA 109 of FIGS. 4A and 4B. At step 502, a common potential (or a common voltage) is maintained at guard electrode 120 and a survey electrode 130a by a source as illustrated in FIGS. 4A and 4B. The common potential may be provided by a voltage source 460 or a current source 470. The common potential may be maintained by direct shorting or by adjusting the guard current 450 using feedback circuitry.

At step 504, a total current is established by the source (the guard electrode 120 and the survey electrode 130a are excited). The total current includes the guard current 450 and the survey current 440. At step 506 a response signal F from the conductive target is measured or determined. The response signal F may be measured by measuring a voltage, a current, a magnetic field (for example, magnetic field 136), an electromagnetic field, or any other characteristic associated with the response signal F. At step 508, the formation current 134 is isolated from the total current.

At step 510, the response signal F received from the conductive target associated with the formation current 134 as determined at step 506 is normalized to obtain a normalized response F'. The normalized response F' may be determined by the ratio of the unnormalized response F and the survey current 440 (I_{survey}), for example, F'=F/I_{survey}. As mentioned above, F' is independent of the resistivity of the

mud **420**. At step **512**, one or more ranging parameters are determining based, at least in part, on the normalized response F' and the survey current **450**. For example, the one or more ranging parameters may be determined based on an inversion algorithm employing a system model. A block diagram for the inversion algorithm is illustrated by FIG. 7. The one or more ranging parameters may include, but are not limited to, a direction α , orientation θ , and distance D of a conductive target. These parameters are found by an optimization (or inversion) algorithm that adjusts a system model until the system model output F'_{model} matches the measured output F' . A cost function is defined as a normalized difference between F'_{model} and F' , which is minimized by the inversion algorithm. The inversion algorithm is usually implemented as a successive iteration that seeks optimal model parameters (α, θ, D) by computing the gradients of the cost function with respect to each model parameter.

If the mud **420** is conductive, F' is essentially independent of the resistivity of the mud. As a result, an inversion algorithm also becomes independent of the mud resistivity. This considerably simplifies the inversion process, as the system model (that which produces the system model output F'_{model}) no longer needs to account for the mud resistivity. In other words, the system model output F'_{model} will be the same regardless of the mud resistivity.

At step **514**, one or more drilling parameters are adjusted based, at least in part, on the determined one or more ranging parameters. The one or more drilling parameters may include, but are not limited to, depth, drilling rate, rotation, torque, thrust pressure, retaining pressure, injection fluid flow rate and pressure, X and Y inclination, and reflected vibration. At step **516**, drilling at the borehole **106** continues based, at least in part, on the one or more adjusted drilling parameters. The method continues from step **516** to step **506** until completion of the drilling operation or may end at any step or at any number of iterations.

FIG. 6 is a flow diagram of an example ranging method, according to aspects of the present disclosure. The ranging method of FIG. 6 may be implemented using any number of configurations for a downhole tool **111**, for example, the BHA **109** of FIG. 4C. FIG. 6 begins after the steps **502**, **504** and **506** as the method of FIG. 6 requires a toroidal coil **490**. At step **602**, the voltage on the toroidal coil **480** (V_{toroid}) is determined so as to determine a mud current flowing through the toroidal coil **490** (I_{gap} , int). For example, I_{gap} , int may be determined as shown in Equation (7) where r is the radius of the toroid from the BHA **109** axis, N is the number of turns for the toroidal coil **490** and A is the tube area for the toroidal coil **490**, μ is the permeability of the toroidal core, and ω is the frequency.

$$I_{gap}, int = \frac{2\pi r}{j\omega\mu NA} V_{toroid} \quad \text{Equation (7)}$$

At step **604**, the entire mud current **434** (I_{gap}) is determined by scaling according to a cross-sectional area of mud flow. For example, the I_{gap} **434** may be determined as shown in Equation (8) where A_{total} is the cross-sectional area of mud flow or the total cross-sectional area of the borehole minus the total cross-sectional area of the body of the BHA **109** and A_{int} is the cross-sectional area of the inside of the BHA **109**.

$$I_{gap} = I_{gap}, int \left(\frac{A_{total}}{A_{int}} \right) \quad \text{Equation (8)}$$

At step **606**, the formation current **134** is determined by removing from the total current the I_{gap} **434**. At step **608**, the measured response signal F received from the conductive target associated with the formation current **134** as determined at step **506** is normalized to obtain a normalized response F' . The normalized response F' may be determined by the ratio of the normalized response F and the formation current **134** as determined at step **606**. The method continues at step **512** as illustrated in FIG. 5.

Any step of FIG. 5 or FIG. 6 may be implemented at any interval time and may occur based, at least in part, on a trigger, occurrence of a condition, a semaphore, an interrupt, according to any other set criteria or any combination thereof. In particular embodiments, the steps of FIG. 5 or FIG. 6 may occur less frequently when a conductive target is determined to be a distance, orientation, direction, or any combination thereof beyond a predefined threshold and may occur more frequently when the conductive target is determined to be a distance, orientation, direction, or any combination thereof within a predetermined threshold. In particular embodiments, the steps of FIG. 5 or FIG. 6 may occur at predetermined time intervals, random time intervals, variable time intervals, user-adjusted time intervals, or any other time interval suitable for a particular environment or operation.

When deployed downhole within a formation **102**, any measurements, calculations determination or other information collection or generated at the downhole tool **111** may then be stored at the downhole tool **111** for later retrieval and processing, or transmitted to a remote information handling system (for example, system control unit **104**), such as an information handling system communicably coupled to the downhole tool **111** through a wireline, for processing in real-time or near real time.

In certain embodiments, an information handling system **200** or a processor **201** may receive at least one of current, voltage, ranging parameters and resistivity measurements from the downhole tool **111** positioned within a borehole **106**. The information handling system **200** may be positioned downhole, such as in the downhole tool **111**, or at the surface **105** (for example, as system control unit **104**).

Any one or more of the aspects of this disclosure provide reducing the effects of mud resistivity on single-well ranging and the interpretation of the received signal F is made easier by removing the effect of conductive mud from the reference current. Any particular embodiment may be well-suited for use of water-based mud in single-well ranging system with electrode excitation, in galvanic ranging, in magnetic ranging and in other ranging scenarios including, but not limited to, well-interception, well-avoidance, and SAGD.

In one or more embodiments a method for downhole ranging within a formation comprises exciting from a source a total current between a survey electrode and a return electrode within a borehole of the formation, wherein the total current comprises a survey current from the source to the survey electrode, and wherein the survey current flows from the survey electrode to the formation, and isolating a formation current from the total current flowing from the survey electrode to the return electrode, wherein the formation current is based, at least in part, on a resistivity of the formation and the survey current, and determining at least one of one or more ranging parameters of a conductive target

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based, at least in part, on the isolated formation current, wherein the at least one of the one or more ranging parameters of the conductive target comprises at least one of distance, orientation, and direction of the conductive target within the formation; and adjusting a drilling operation based, at least in part, on the determined at least one of the one or more ranging parameters of the conductive target.

In one or more embodiments the method for downhole ranging within a formation further comprises measuring a receive signal at a receiver, wherein the receive signal is associated with the conductive target, and normalizing the receive signal, wherein the adjusting the drilling operation is based, at least in part, on a ranging model that comprises the at least one of the one or more ranging parameters. In one or more embodiments the method for downhole ranging within a formation further comprises maintaining a common voltage at a guard electrode and the survey electrode, and determining a gap current, wherein the gap current flows from the guard electrode to the return electrode, and wherein the guard electrode is located between the survey electrode and the return electrode, wherein isolating the formation current is based, at least in part, on the gap current and the survey current. In one or more embodiments the method for downhole ranging within a formation further comprises isolating the survey current and a guard current via a first gap sub, wherein the first gap sub is located between the survey electrode and the guard electrode, and wherein the guard current flows from the source to the guard electrode. In one or more embodiments the method for downhole ranging within a formation further comprises isolating the return electrode via a second gap sub between the guard electrode and the return electrode, wherein the second gap sub prevents current from flowing through the tool from the guard electrode to the return electrode. In one or more embodiments the method for downhole ranging within a formation further comprises maintaining a potential at the guard electrode and the survey electrode via a feedback loop and adjusting the guard current based, at least in part, on the feedback loop.

In one or more embodiments the method for downhole ranging within a formation further comprises isolating the survey electrode from the return electrode via a gap sub between the survey electrode and the return electrode, and determining a gap current via a toroidal coil wrapped around the gap sub, wherein the gap current flows through a mud inside an assembly from the survey electrode through the gap sub to the return electrode, wherein the gap sub is located between the survey electrode and the return electrode, and wherein the tool is within the assembly, and scaling the gap current, and determining a formation current based, at least in part, on the total current and the gap current, wherein normalizing the received signal is based, at least in part, on the formation current, and wherein determining the at least one of the one or more parameters of the conductive target is based, at least in part, on the normalized received signal. In one or more embodiments the method for downhole ranging within a formation further comprises wherein scaling the gap current is based, at least in part, on a ratio of a total cross-sectional area of mud flow within the borehole to a cross-sectional area of an inside of the assembly. In one or more embodiments the method for downhole ranging within a formation further comprises wherein the adjusting the drilling operation is based, at least in part, on a model, wherein the model is independent of mud resistivity.

In one or more embodiments, a wellbore drilling system for drilling in a subsurface earth formation, comprises a

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ranging tool coupled to a drill string, and a survey electrode coupled to the ranging tool, and a return electrode coupled to the ranging tool, and an information handling system communicably coupled to the ranging tool, the information handling system comprises a processor and memory device coupled to the processor, the memory device containing a set of instruction that, when executed by the processor, cause the processor to excite from a source a total current between the survey electrode and the return electrode within a borehole of the earth formation, wherein the total current comprises a survey current from the source to the survey electrode, and wherein the survey current flows from the survey electrode to the formation, and isolate a formation current from the total current flowing from the survey electrode to the return electrode, wherein the formation current is based, at least in part, on a resistivity of the formation and the survey current, and determine at least one of one or more ranging parameters of a conductive target based, at least in part, on the isolated formation current, wherein the at least one of the one or more ranging parameters of the conductive target comprises at least one of distance, orientation, and direction of the conductive target within the formation, and adjust a drilling operation of the wellbore drilling system based, at least in part, on the determined at least one parameter of the conductive target.

In one or more embodiments, the wellbore drilling system for drilling in a subsurface earth formation, further comprises a receiver coupled to the ranging tool, and wherein the set of instructions further cause the processor to measure a receive signal at a receiver, wherein the receive signal is associated with the conductive target, and normalize the receive signal, wherein the adjusting the drilling operation is based, at least in part, on a ranging model that comprises the at least one of the one or more ranging parameters. In one or more embodiments, the wellbore drilling system for drilling in a subsurface earth formation further comprises, wherein the guard electrode is located between the survey electrode and the return electrode, and wherein the set of instructions further cause the processor to maintain a common voltage at a guard electrode and the survey electrode, and determine a gap current, wherein the gap current flows from the guard electrode to the return electrode, and wherein isolating the formation current is based, at least in part, on the gap current and the survey current. In one or more embodiments, the wellbore drilling system for drilling in a subsurface earth formation, further comprises a first gap sub located between the survey electrode and the guard electrode, and wherein the set of instructions further cause the processor to isolate the survey current and a guard current via the first gap sub, wherein the guard current flows from the source to the guard electrode.

In one or more embodiments, the wellbore drilling system for drilling in a subsurface earth formation, further comprises, wherein the set of instructions further cause the processor to isolate the return electrode via a second gap sub between the guard electrode and the return electrode, wherein the second gap sub prevents current from flowing through the tool from the guard electrode to the return electrode. In one or more embodiments, the wellbore drilling system for drilling in a subsurface earth formation, further comprises, wherein the set of instructions further cause the processor to maintain a potential at the guard electrode and the survey electrode via a feedback loop, and adjust the guard current based, at least in part, on the feedback loop. In one or more embodiments, the wellbore drilling system for drilling in a subsurface earth formation, further comprises, a gap sub between the survey electrode and the return elec-

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trode, and a toroidal coil wrapped around the gap sub, and wherein the set of instructions further cause the processor to isolate the survey electrode from the return electrode via the gap sub between the survey electrode and the return electrode, and determine a gap current via the toroidal coil, wherein the gap current flows through a mud inside an assembly from the survey electrode through the gap sub to the return electrode, wherein the gap sub is located between the survey electrode and the return electrode, and wherein the ranging tool is within the assembly, and scale the gap current, and determine a formation current based, at least in part, on the total current and the gap current, and

wherein normalizing the received signal is based, at least in part, on the formation current, and wherein determining the at least one of the one or more parameters of the conductive target is based, at least in part, on the normalized received signal.

In one or more embodiments, the wellbore drilling system for drilling in a subsurface earth formation, further comprises, wherein the set of instructions further cause the processor to when scaling the gap current, to scale the gap current based, at least in part, on a ratio of a total cross-sectional area of mud flow within the borehole to a cross-sectional area of an inside of the assembly. In one or more embodiments, the wellbore drilling system for drilling in a subsurface earth formation, further comprises, wherein the set of instructions further cause the processor to exclude mud resistivity when determining the at least one of the one or more ranging parameters.

In one or more embodiments, A non-transitory computer readable medium storing a program that, when executed, causes a processor to excite from a source a total current between a survey electrode and a return electrode within a borehole of a formation, wherein the total current comprises a survey current from the source to the survey electrode, and wherein the survey current flows from the survey electrode to the formation, and isolate a formation current from the total current flowing from the survey electrode to the return electrode, wherein the formation current is based, at least in part, on a resistivity of the formation and the survey current, and determine at least one of one or more ranging parameters of a conductive target based, at least in part, on the isolated formation current, wherein the at least one of the one or more ranging parameters of the conductive target comprises at least one of distance, orientation, and direction of the conductive target within the formation, and adjust a drilling operation based, at least in part, on the determined at least one or more ranging parameters of the conductive target. In one or more embodiments, the non-transitory computer readable medium further comprises, wherein the program, when executed, causes the processor to measure a receive signal at a receiver, wherein the receive signal is associated with the conductive target, normalize the receive signal, and wherein the adjusting the drilling operation is based, at least in part, on a ranging model that comprises the at least one of the one or more ranging parameters.

Therefore, the present disclosure is well adapted to attain the ends and advantages mentioned as well as those that are inherent therein. The particular embodiments disclosed above are illustrative only, as the present disclosure may be modified and practiced in different but equivalent manners apparent to those skilled in the art having the benefit of the teachings herein. Furthermore, no limitations are intended to the details of construction or design herein shown, other than as described in the claims below. It is therefore evident that the particular illustrative embodiments disclosed above may be altered or modified and all such variations are considered

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within the scope and spirit of the present disclosure. Also, the terms in the claims have their plain, ordinary meaning unless otherwise explicitly and clearly defined by the patentee. The indefinite articles "a" or "an," as used in the claims, are defined herein to mean one or more than one of the element that it introduces.

What is claimed is:

1. A method for downhole ranging within a formation, the method comprising:

exciting from a source a total current between a survey electrode at a first location of a tool and a return electrode located at a second location of the tool within a borehole of the formation, wherein the total current comprises a survey current from the source to the survey electrode, and wherein the survey current flows from the survey electrode to the formation;

isolating a formation current from the total current flowing from the survey electrode to the return electrode, wherein the formation current is based, at least in part, on a resistivity of the formation and the survey current; isolating, by a guard electrode located between the survey electrode and the return electrode, a gap current from the total current;

determining at least one of one or more ranging parameters of a conductive target based, at least in part, on the isolated formation current, wherein the at least one of the one or more ranging parameters of the conductive target comprises at least one of distance, orientation, direction or any combination thereof of the conductive target within the formation; and

adjusting a drilling operation based, at least in part, on the determined at least one of the one or more ranging parameters of the conductive target.

2. The method of claim 1 further comprising:

measuring a receive signal at a receiver, wherein the receive signal is associated with the conductive target; normalizing the receive signal; and

wherein the adjusting the drilling operation is based, at least in part, on a ranging model that comprises the at least one of the one or more ranging parameters.

3. The method of claim 2, further comprising:

isolating the survey electrode from the return electrode via a gap sub between the survey electrode and the return electrode;

determining a gap current via a toroidal coil wrapped around the gap sub, wherein the gap current flows through a mud inside an assembly from the survey electrode through the gap sub to the return electrode, wherein the gap sub is located between the survey electrode and the return electrode, and wherein the tool is within the assembly;

scaling the gap current;

determining a formation current based, at least in part, on the total current and the gap current;

wherein normalizing the received signal is based, at least in part, on the formation current; and

wherein determining the at least one of the one or more parameters of the conductive target is based, at least in part, on the normalized received signal.

4. The method of claim 3, further comprising:

wherein scaling the gap current is based, at least in part, on a ratio of a total cross-sectional area of mud flow within the borehole to a cross-sectional area of an inside of the assembly.

5. The method of claim 1 further comprising:

maintaining a common voltage at the guard electrode and the survey electrode;

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determining the gap current, wherein the gap current flows from the guard electrode to the return electrode, and wherein the guard electrode is located between the survey electrode and the return electrode; and wherein isolating the formation current is based, at least in part, on the gap current and the survey current. 5

6. The method of claim 5, further comprising: isolating the survey current and a guard current via a first gap sub, wherein the first gap sub is located between the survey electrode and the guard electrode, and wherein the guard current flows from the source to the guard electrode. 10

7. The method of claim 5, further comprising: isolating the return electrode via a second gap sub between the guard electrode and the return electrode, wherein the second gap sub prevents current from flowing through the tool from the guard electrode to the return electrode. 15

8. The method of claim 5, further comprising: maintaining a potential at the guard electrode and the survey electrode via a feedback loop; and adjusting the guard current based, at least in part, on the feedback loop. 20

9. The method of claim 1, further comprising: wherein the adjusting the drilling operation is based, at least in part, on a model, wherein the model is independent of mud resistivity. 25

10. A wellbore drilling system for drilling in a subsurface earth formation, comprising: 30

- a ranging tool coupled to a drill string;
- a survey electrode coupled to the ranging tool at a first location;
- a return electrode coupled to the ranging tool at a second location; and
- an information handling system communicably coupled to the ranging tool, the information handling system comprises a processor and memory device coupled to the processor, the memory device containing a set of instruction that, when executed by the processor, cause the processor to: 40

- excite from a source a total current between the survey electrode and the return electrode within a borehole of the earth formation, wherein the total current comprises a survey current from the source to the survey electrode, and wherein the survey current flows from the survey electrode to the formation;
- isolate a formation current from the total current flowing from the survey electrode to the return electrode, wherein the formation current is based, at least in part, on a resistivity of the formation and the survey current; 50
- isolate, by a guard electrode located between the survey electrode and the return electrode, a gap current from the total current;
- determine at least one of one or more ranging parameters of a conductive target based, at least in part, on the isolated formation current, wherein the at least one of the one or more ranging parameters of the conductive target comprises at least one of distance, orientation, direction or any combination thereof of the conductive target within the formation; and 60
- adjust a drilling operation of the wellbore drilling system based, at least in part, on the determined at least one parameter of the conductive target.

11. The wellbore drilling system of claim 10, further comprising: 65

- a receiver coupled to the ranging tool; and

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wherein the set of instructions further cause the processor to:

- measure a receive signal at a receiver, wherein the receive signal is associated with the conductive target;
- normalize the receive signal; and
- wherein the adjusting the drilling operation is based, at least in part, on a ranging model that comprises the at least one of the one or more ranging parameters.

12. The wellbore drilling system of claim 11 further comprising:

- a gap sub between the survey electrode and the return electrode;
- a toroidal coil wrapped around the gap sub; and
- wherein the set of instructions further cause the processor to: 5

- isolate the survey electrode from the return electrode via the gap sub between the survey electrode and the return electrode;
- determine a gap current via the toroidal coil, wherein the gap current flows through a mud inside an assembly from the survey electrode through the gap sub to the return electrode, wherein the gap sub is located between the survey electrode and the return electrode, and wherein the ranging tool is within the assembly;
- scale the gap current;
- determine a formation current based, at least in part, on the total current and the gap current;
- wherein normalizing the received signal is based, at least in part, on the formation current; and
- wherein determining the at least one of the one or more parameters of the conductive target is based, at least in part, on the normalized received signal.

13. The wellbore drilling system of claim 12, wherein the set of instructions further cause the processor to:

- when scaling the gap current, to scale the gap current based, at least in part, on a ratio of a total cross-sectional area of mud flow within the borehole to a cross-sectional area of an inside of the assembly.

14. The wellbore drilling system of claim 10, wherein the guard electrode is located between the survey electrode and the return electrode, and wherein the set of instructions further cause the processor to: 10

- maintain a common voltage at the guard electrode and the survey electrode;
- determine the gap current, wherein the gap current flows from the guard electrode to the return electrode; and
- wherein isolating the formation current is based, at least in part, on the gap current and the survey current.

15. The wellbore drilling system of claim 14, further comprising:

- a first gap sub located between the survey electrode and the guard electrode; and
- wherein the set of instructions further cause the processor to: 15

- isolate the survey current and a guard current via the first gap sub, wherein the guard current flows from the source to the guard electrode.

16. The wellbore drilling system of claim 14, wherein the set of instructions further cause the processor to:

- isolate the return electrode via a second gap sub between the guard electrode and the return electrode, wherein the second gap sub prevents current from flowing through the tool from the guard electrode to the return electrode.

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17. The wellbore drilling system of claim 14, wherein the set of instructions further cause the processor to:
 maintain a potential at the guard electrode and the survey electrode via a feedback loop; and
 adjust the guard current based, at least in part, on the feedback loop.

18. The wellbore drilling system of claim 10, wherein the set of instructions further cause the processor to:
 exclude mud resistivity when determining the at least one of the one or more ranging parameters.

19. A non-transitory computer readable medium storing a program that, when executed, causes a processor to:
 excite from a source a total current between a survey electrode at a first location and a return electrode at a second location within a borehole of a formation, wherein the total current comprises a survey current from the source to the survey electrode, and wherein the survey current flows from the survey electrode to the formation;

isolate a formation current from the total current flowing from the survey electrode to the return electrode, wherein the formation current is based, at least in part, on a resistivity of the formation and the survey current;

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isolate, by a guard electrode located between the survey electrode and the return electrode, a gap current from the total current, wherein;

determine at least one of one or more ranging parameters of a conductive target based, at least in part, on the isolated formation current, wherein the at least one of the one or more ranging parameters of the conductive target comprises at least one of distance, orientation, direction or any combination thereof of the conductive target within the formation; and

adjust a drilling operation based, at least in part, on the determined at least one or more ranging parameters of the conductive target.

20. The non-transitory computer readable medium of claim 19, wherein the program, when executed, causes the processor to:

measure a receive signal at a receiver, wherein the receive signal is associated with the conductive target;

normalize the receive signal; and

wherein the adjusting the drilling operation is based, at least in part, on a ranging model that comprises the at least one of the one or more ranging parameters.

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